

1 Article

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A Hybrid Lagrangian-Eulerian Particle Model for

3

Ecosystem Simulation

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11 **Abstract:** Current numerical methods for simulating biophysical processes in aquatic environments
 12 are typically constructed in a grid-based Eulerian framework using the advection-diffusion
 13 equation for physical transport with source and sink terms describing biological processes. Often,
 14 the biogeochemical processes and physical (hydrodynamic) processes occur at different time and
 15 space scales, and changes in biological processes do not affect the hydrodynamic conditions.
 16 Therefore, it is possible to develop an alternative strategy to grid-based approaches for linking
 17 hydrodynamic and biogeochemical models that can significantly improve computational efficiency
 18 for this type of linked biophysical model. In this work, we utilize a new technique which links
 19 hydrodynamic effects and biological processes through a property-carrying particle model (PCPM)
 20 in a Lagrangian/Eulerian framework. The model is tested in idealized cases and its utility is
 21 demonstrated in a practical application to Sandusky Bay. Results show the integration of
 22 Lagrangian and Eulerian approaches allows for a natural coupling of mass transport (represented
 23 by particle movements and random walk) and biological processes in water columns which is
 24 described by a nutrient-phytoplankton-zooplankton-detritus (NPZD) biological model. This
 25 method is far more efficient than traditional tracer based Eulerian biophysical models for 3-D
 26 simulation, particularly for a large domain and/or ensemble simulations.

27 **Keywords:** Property-carrying Particle Model; Ecosystem Simulation; Biophysical Modeling;
 28 Sandusky Bay; Great Lakes

29

1. Introduction

30 Current numerical methods for simulating biogeochemical processes in aquatic environments
 31 are typically constructed in a grid-based Eulerian framework. Equations for the time evolution of
 32 state variables of the biophysical model include advection and diffusion terms which depend on
 33 hydrodynamic variables, as well as source and sink terms representing growth, decay, and
 34 interaction with other biogeochemical variables. The property concentration fields ($C_i, i = 1, 2, 3, \dots$)
 35 are often calculated using a set of advection-diffusion equations:

$$36 \quad \frac{\partial D C_i}{\partial t} + \frac{\partial D u C_i}{\partial x} + \frac{\partial D v C_i}{\partial y} + \frac{\partial D w C_i}{\partial z} - \frac{1}{D} \frac{\partial}{\partial z} \left(K_h \frac{\partial C_i}{\partial z} \right) - D F_c = C_{i,source} - C_{i,sink} \quad (1)$$

37 where D is the total water depth, u, v , and w are the x, y , and z components of the water velocity,
 38 K_h is the vertical thermal diffusion coefficient, F_c is the horizontal diffusion term, and $C_{i,source}$ and
 39 $C_{i,sink}$ represents the sources and sinks of C_i , respectively, due to the biological processes which are
 40 typically described using a set of biological process equations. This approach has been widely used
 41 in coastal and ocean modeling communities [e.g. 1-4].

42 A major practical challenge is that the biological submodel often involves a large group of
 43 parameters for calibration and confirmation which requires a considerable amount of computational
 44 time to tune the model. As shown in Equation 1, tuning the simulation of biological processes (e.g.
 45 changes in parameterization, initial and boundary conditions) requires a complete time integration

46 of the entire equation so that the impact of physical process (advection and diffusion) on the
47 biological properties can be properly incorporated. However, the biophysical process is generally not
48 two-way coupled. In other words, one can often assume that changes in biological processes (in our
49 case, the resulting changes in NPZD property concentration) do not affect the hydrodynamic
50 condition (currents, temperature, mixing, etc.). This indicates that there may be a more
51 computationally efficient approach to resolve the impact of hydrodynamics on the biological
52 processes rather than directly integrate Equation 1 every time the biological submodel is tuned.

53 The PCPM is developed to test the feasibility of an alternative strategy to grid-based approaches
54 for linking hydrodynamic and biogeochemical models that may reduce the problems mentioned
55 above. Instead of grid-based, time-averaging of hydrodynamic variables, the hydrodynamic model
56 is used to calculate the Lagrangian trajectories of a large number of current-following tracer particles;
57 these trajectories become the linking mechanism between the hydrodynamic model and the
58 biogeochemical model. In hybrid Lagrangian-Eulerian PCPM, each current-following tracer particle
59 carries with it a number of time-varying properties which correspond to the state variables of the
60 biogeochemical model. The PCPM also employs its own horizontal grid system or series of regions
61 which is independent of the hydrodynamic model grid and is used to calculate local average values
62 of the particle-based properties. These cell-based properties allow all particles within a PCPM cell to
63 influence the properties of other particles within the same cell or region and allow for display and
64 analysis of biogeochemical fields.

65 The remaining sections of this paper are organized as follows: Details of PCPM are described in
66 section 2. The results and discussion of two idealized experiments are presented in section 3. The
67 application of PCPM to Sandusky Bay is presented in section 4. A discussion and summary of the
68 PCPM is concluded in section 5.

69 2. Methods

70 In this implementation of PCPM, particle trajectories are pre-computed based on the output of
71 a hydrodynamic model and are independent of the particle properties. An initial particle density (i.e.,
72 total number of particles / volume of computational domain) is selected and particles are randomly
73 distributed throughout the computational domain. Particles are not allowed to leave the
74 computational domain except at hydrodynamic outflows. At hydrodynamic inflows, new particles
75 are introduced with the same density as the initial distribution. The total number of active particles
76 is not strictly preserved, but if there is a net balance of hydrodynamic inflows and outflows, the total
77 number of particles is approximately constant.

78 An alternative approach to implementing a PCPM would allow particle-based properties to
79 influence particle trajectories, perhaps through buoyancy or sinking. In this case, the PCPM would
80 have to be directly coupled with the particle trajectory calculation. In the initial implementation of
81 PCPM this paper, we consider only the uncoupled case.

82 Any suitable method can be used to generate the Lagrangian particle trajectories. Typically, the
83 trajectories are calculated from a time integration of the Lagrangian equations of motion:

$$84 \quad \frac{dx}{dt} = u, \frac{dy}{dt} = v, \frac{dz}{dt} = w \quad (2)$$

85 where (x, y, z) is the particle's position in 3 dimensions, (u, v, w) is the local fluid velocity vector, and t
86 is time. For the two idealized examples presented in this paper, the trajectories are calculated semi-
87 analytically from a simple, idealized flow field. The third, more realistic example, demonstrates the
88 use of a full hydrodynamic model of a natural basin (i.e., Sandusky Bay) to compute currents and
89 trajectories.

90 PCPM uses a computational grid system which is independent of the grid system used to
91 compute currents for particle trajectories. The PCPM computational cells are used to define regions
92 in which the properties carried by the particles are allowed to interact with one another. In this
93 respect, PCPM is similar to the classic Particle-in-Cell (PIC) method with PM (particle-mesh)
94 interactions. PIC methods can also be mesh-independent by allowing direct particle-particle (PP)
95 interactions, or a combination of PM and PP [5-8]. In PCPM, a basic simplifying assumption is that

96 only particles within a single PCPM cell are allowed to interact, such as the PIC PM method. The
97 advantage of this approach is that it is conceptually intuitive to implement and computationally
98 efficient to program.

99 Each computational time step in the PCPM consists of six intermediate steps:

- 100 1. Read particle locations (x, y, z) and temperature at this location for all tracer particles at this time
101 step. Locations are pre-computed based on currents from a hydrodynamic model.
- 102 2. Determine the PCPM cell for each particle. Cells can be 2-D or 3-D.
- 103 3. Apply boundary conditions to any particle-based properties that require them.
- 104 4. Calculate PCPM cell-based average of each property.
- 105 5. Calculate the time evolution of the cell-based properties (and particle-based properties, if
106 necessary) using the process equations defined for that property.
- 107 6. Redistribute cell-based properties to particles within each cell by replacing the particle-based
108 property with a weighted average of the particle-based property and the new cell-based
109 property.

110 Note that all steps except 3 and 5 are independent of the specific problem, i.e., they will be carried
111 out the same way no matter how many properties are attached to the particles or what those
112 properties represent. More importantly, steps 1 and 2 only need to be run once regardless of
113 modifications in biological processes at the later stage. These are two of the key designs of PCPM for
114 the enhanced computational efficiency.

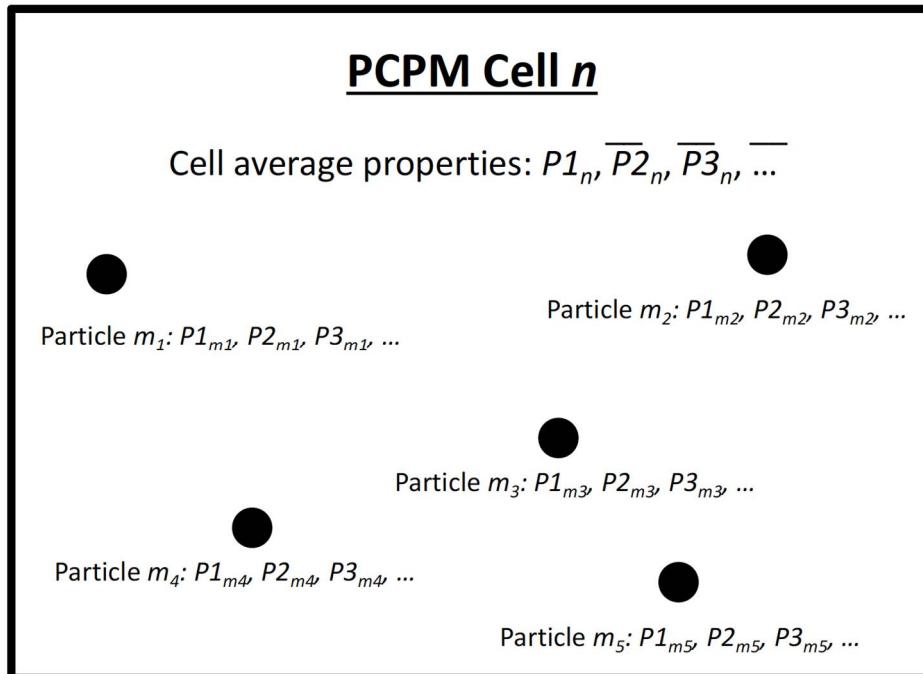
115 Consider each of these steps in detail:

- 116 1. Read particle locations (x, y, z) and temperature. This step simply updates the location of each
117 particle that is being used in the computation. Figure 1 is a conceptual representation of a PCPM
118 computational cell. Particles (m_1, m_2, m_3, \dots) move in and out of the cell at each PCPM time step
119 based on their trajectories as computed from the hydrodynamic model. The total number of
120 particles for a particular computation is assumed to be fixed for the duration of the computation,
121 although some particles may enter or leave the PCPM domain during the computation. Water
122 temperature or other physical properties from the hydrodynamic calculation can be stored along
123 with the pre-computed particle trajectories and can be included as one of the properties ($P_1, P_2,$
124 P_3, \dots) carried by the particle.
- 125 2. Determine the PCPM cell for each particle. In Figure 1, the PCPM cell is represented by the
126 enclosing rectangle. The PCPM domain need not coincide with the domain that was used for the
127 hydrodynamic simulation and computation of particle trajectories. It can be regular or irregular,
128 as long as there is a prescribed method to calculate which PCPM cell contains a prescribed
129 particle position (x, y, z). The PCPM cells are the volumes within which particle properties can
130 interact, that is, during a single time step, all particles within a PCPM cell can influence the
131 evolution of particle properties within that cell, but are independent of other cells.
- 132 3. Apply boundary conditions to any particle-based properties that require them. If there is a
133 property (e.g., concentration of a dissolved nutrient) that needs to be specified as a boundary
134 condition, then particles within the cell where the boundary condition needs to be applied will
135 have that property adjusted to meet the boundary condition. For example, in a cell that is
136 associated with an inflow to the domain, the properties that are being carried into the domain
137 through the inflow are adjusted to take account of the change in that property for particles within
138 that cell. Alternatively, if particles from the hydrodynamic-based trajectory calculation are
139 entering a PCPM cell, the values of the associated properties for each particle need to be
140 specified.
- 141 4. Calculate PCPM cell-based averages of each property. In this step, the averages of K_{th} property
142 for cell n are calculated as

$$\overline{PK_n} = \sum_{j=1}^L PK_{m_j}/L \quad (3)$$

144 where the summation includes all L particles (m_1, m_2, \dots, m_L) currently within cell n . L is the
145 number of particles within that cell. If no particles are present in a particular cell, PCPM uses the
146 values of $\overline{PK_n}$ from the previous time step.

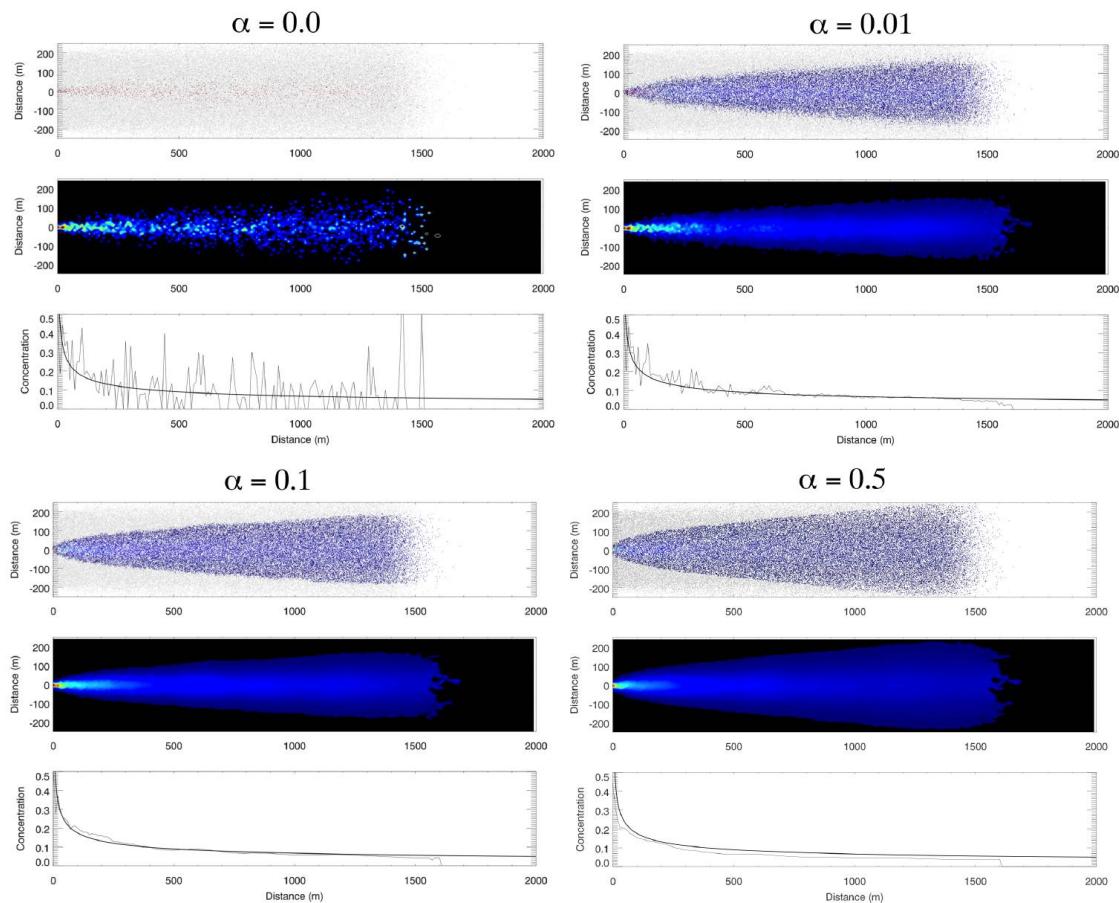
147 5. Calculate the time evolution of the cell-based properties (and particle-based properties if
 148 necessary) using the process equation defined for that property. The process equations can
 149 incorporate terms which depend on either particle-based or cell-based properties, or both, i.e.
 150 $\overline{PK_n(t + \Delta t)} = FN(P1_M(t), P2_M(t), P3_M(t), \dots, \overline{P1_n}(t), \overline{P2_n}(t), \overline{P3_n}(t), \dots)$ (4)
 151 Note that M indicates m_1, m_2, \dots, m_L . The form of FN is completely general and depends on the
 152 problem being solved. For instance, in a NPZD model, the P_i , ($i = 1, 2, 3, \dots$) would be N, P, Z, D,
 153 and water temperature, and the FN would be the process equations relating these properties.
 154 Since the cell-based averages have already been computed, the right-hand side of equation 4 is
 155 independent of the left-hand side, so the computation of the evolution equations can be carried
 156 out in parallel. This is another key design feature of PCPM allowing it to take full advantage of
 157 multiprocessing computer environments, both Symmetric Multi-Processing (SMP) and
 158 Massively Parallel Processing (MPP).
 159 6. Redistribute cell-based properties to particles within each cell by replacing the particle-based
 160 property with a weighted average of the cell-based property. After the evolution equations have
 161 been carried out (Step 5), particles within an individual cell most likely carry a range of different
 162 values of the various properties, which vary around the new cell-based average computed in
 163 Step 5, $\overline{PK_n(t + \Delta t)}$. PCPM provides an optional step to reduce the variance of the new particle-
 164 based properties within each cell. This optional step is applied as a 'nudging' term, i.e.
 165 $PK_m(t + \Delta t) = (1 - \alpha_i)PK_m(t) + \alpha_i\overline{PK_n(t + \Delta t)}$ (5)
 166 where $0 < \alpha_i < 1$ is the redistribution weight (i.e. nudging) factor. If $\alpha_i = 0$, no adjustment is carried
 167 out and particle-based property remain unchanged. If $\alpha_i = 1$, then all particles within a cell are
 168 assigned the cell-based average of that property. This step can be useful to smooth results when
 169 limited particle density results in excessive within-cell variability.



170
 171 **Figure 1.** Conceptual representation of a PCPM computational cell n and particles ($m_1, m_2, m_3, m_4, m_5, \dots$)
 172 within the cell n. PCPM cell-based average of each property ($\overline{P1_n}, \overline{P2_n}, \overline{P3_n}, \dots$) is determined by the
 173 property values carried by the particles that have entered in this cell. After time evolution of PCPM
 174 properties using process equations, the updated PCPM cell-based properties ($\overline{P1_n}, \overline{P2_n}, \overline{P3_n}, \dots$) are
 175 redistributed to particles with a weighted average. Then the particles move around carrying the
 176 updated properties to different PCPM computational cell in the next cycle.
 177

178 **3. Results of Idealized Cases**179 **3.1. Advection-diffusion plume**

180 In PCPM, diffusion is provided mainly by particle trajectories, although the cell-based averaging
 181 of particle properties and the (optional) redistribution of cell-based properties to particles within the
 182 cell can also act as diffusive terms. To demonstrate the effect of particle trajectory diffusion on particle
 183 properties, we constructed a 500 m wide x 2000 m long channel divided into 10 m square cells (Fig.
 184 2). Particles were introduced at random locations along the center 400 m section of the left edge of
 185 the channel at the rate of 100/sec. The particles were assigned an along-channel velocity of 2 m/sec.
 186 Horizontal diffusion was added using a random-walk perturbation to the particle trajectories of
 187 $2r\sqrt{2k_h\Delta t}$ in both cross-channel and long-channel directions. Here, r is a uniformly distributed
 188 random number in the range [-1,1], k_h is the horizontal diffusion coefficient (10 m²/sec in this
 189 experiment), and Δt is the time step for the particle trajectory calculation (1 sec).



190

191 **Figure 2.** PCPM simulation of concentration plume in an idealized channel with four different values
 192 of the cell-based redistribution weight parameter ($\alpha = 0, 0.01, 0.1, 0.5$). There are three panels for each
 193 value of α . The top panel shows the locations of particles after 720 time steps (12 minutes). The second
 194 panel shows the average concentration in each 10 m square cell with the same blue to red scale as the
 195 top panel, except cells with $C = 0$ are black. The third panel compares concentration along the
 196 centerline of the plume to the analytical solution for a diffusive plume.

197 In this example, PCPM particles carry only one property, concentration ($P1=C$), and there is no
 198 time evolution equation (step 5, above). The purpose of this example is to illustrate how PCPM
 199 simulates horizontal diffusion through a combination of the particle trajectories and the cell-based
 200 averaging in step 6. To simulate a concentration plume, particles introduced in the center of the left
 201 wall (-50 m < y < 50 m) are assigned the initial condition $C = 1$. Particles entering the channel outside

202 this region have an initial condition of $C = 0$. To illustrate the effect of the cell-based averaging (step
 203 6), we show results for four different values of the cell-based redistribution parameter ($\alpha = 0, 0.01,$
 204 $0.1, 0.5$) in Figure 2. In Figure 2, there are three panels for each value of α . The top panel shows the
 205 locations of particles after 720 time steps (12 minutes). The particles are colored using a blue-to-red
 206 scale for concentration values from 0 to 1. Particles with a concentration value of exactly 0 are colored
 207 light gray. The second panel shows the average concentration in each 10 m square cell with the same
 208 blue to red scale as the top panel, except cells with $C = 0$ are black. The third panel compares
 209 concentration along the centerline of the plume from the second panel to the analytical solution for a
 210 diffusive plume [9,10], i.e.,

$$211 \quad C(x) = \text{erf}\left(\left[\frac{2}{3}([1.4x + 1]^{0.833} - 1)\right]^{-0.5}\right) \quad (6)$$

212 where $C(x)$ is the centerline concentration x meter away from the channel entrance. In the case $\alpha =$
 213 0, there is no cell-based redistribution of properties, so all particles retain their initial concentration
 214 values of either $C=0$ (light gray in panel 1) or $C=1$ (red in panel 1). As seen in the second and third
 215 panels, the random-walk diffusion in the particle trajectories does provide a rough approximation to
 216 the analytical solution by mixing of $C=0$ and $C=1$ particles in PCPM cells. Of course increasing the
 217 number of particles in the simulation would provide a more accurate approximation, but would also
 218 increase the computational load. Setting the cell-based redistribution parameter to even the small
 219 value of $\alpha = 0.01$ provides a significant improvement in the solution with the same number of
 220 particles, particularly for $x > 500$ m. Now particles can have any value of C between 0 and 1.
 221 Increasing the redistribution parameter to $\alpha = 0.1$ further improves the solution for $x < 500$ m. Further
 222 increasing α to 0.5 does not significantly improve the solution in comparison to $\alpha = 0.1$.

223 *3.2. Vertical settling*

224 Since this implementation of PCPM does not allow the properties carried by the particles to
 225 influence particle trajectories, the question arises of how to simulate the vertical transport of a
 226 property when the vertical transport depends on the property itself, such as sediment settling or
 227 biologically generated buoyancy. In PCPM, the answer is simply to solve the vertical transport at the
 228 PCPM cell-based Eulerian framework in step 5 as a traditional cell-based method. Interaction of
 229 particle properties with adjacent cell averages is technically not allowed in the basic PCPM
 230 framework, but an exception is made in this case. The vertical advection-diffusion equation for
 231 sediment concentration is shown below

$$232 \quad \frac{\partial C}{\partial t} = w_s \frac{\partial C}{\partial z} + k_z \frac{\partial^2 C}{\partial z^2} \quad (7)$$

233 where w_s is the bulk settling velocity of the suspended material and k_z is the vertical diffusion
 234 coefficient.

235 Since vertical diffusion is already included in the particle trajectories, PCPM only needs to
 236 consider the first term on the right-hand side of (7) to account for the additional vertical transport
 237 that depends on the property itself. To implement this term in PCPM, the process equation for a
 238 particle carrying a property C_m in vertical cell k looks like

$$239 \quad C_m(t + \Delta t) = C_m(t) + w_s \Delta t (\overline{C_{k-1}(t)} - \overline{C_k(t)}) \Delta z + (\text{other process terms}) \quad (8)$$

240 where $\overline{C_k(t)}$ is the average concentration in vertical cell k , $\overline{C_{k-1}(t)}$ is the average concentration in
 241 the next higher vertical cell, and Δz is the spacing between the centers of the cells. For particles in
 242 the top cell ($k=0$), we set

$$243 \quad C_m(t + \Delta t) = C_m(t) - w_s \Delta t \overline{C_0(t)} \Delta z + (\text{other process terms}) \quad (9)$$

244 and for particles in the bottom cell ($k=k_{max}$), we set

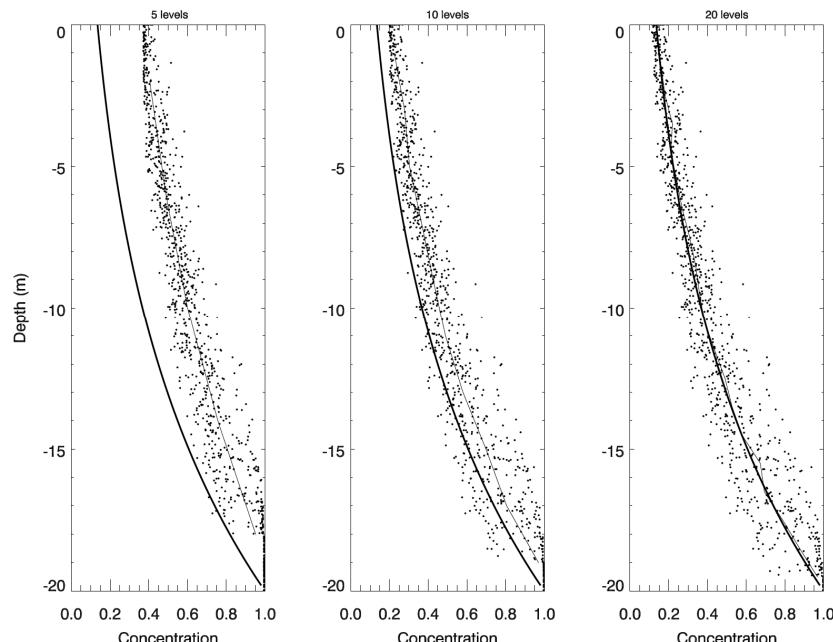
$$245 \quad C_m(t + \Delta t) = C_m(t) - w_s \Delta t \overline{C_{k_{max}}(t)} \Delta z + (\text{other process terms}) \quad (10)$$

246 As a test case, we examine the vertical setting in a one-dimensional water column of depth d with
 247 particles moving vertically only through vertical diffusion. Particles are initially distributed
 248 randomly in the column and then move with a random walk velocity of $2r\sqrt{2k_z\Delta t}$ where r is a
 249 uniformly distributed random number in the range [-1,1] and k_z is the vertical diffusion coefficient.
 250 Particles are not allowed to cross the surface or bottom boundaries. Thus, in this experiment, the
 251 number of particles is constant and are always approximately uniformly distributed in the vertical
 252 due to vertical mixing.

253 For the experiment, we set $C = 1$ as the bottom boundary condition by assigning this value at the
 254 beginning of each time step to all particles in the lower half of the bottom cell. The initial condition
 255 in other cells is $C = 0$. For the test case, we set the number of particles to 1000, $d = 20$ m, $k_z = 10^{-4}$ m²s⁻¹,
 256 and the redistribution parameter $\gamma = 0.1$. Three runs were made with 5, 10, and 20 vertical cells
 257 respectively. PCPM is integrated in time with $\Delta t = 1$ hr. The results at the end of 5,000 time steps are
 258 shown in Figure 3. In Figure 3, the dots represent the locations of the particles on the vertical axis and
 259 the value of concentration they are carrying on the horizontal axis. The thin line is the cell average
 260 concentration. The thick line is the analytical solution,

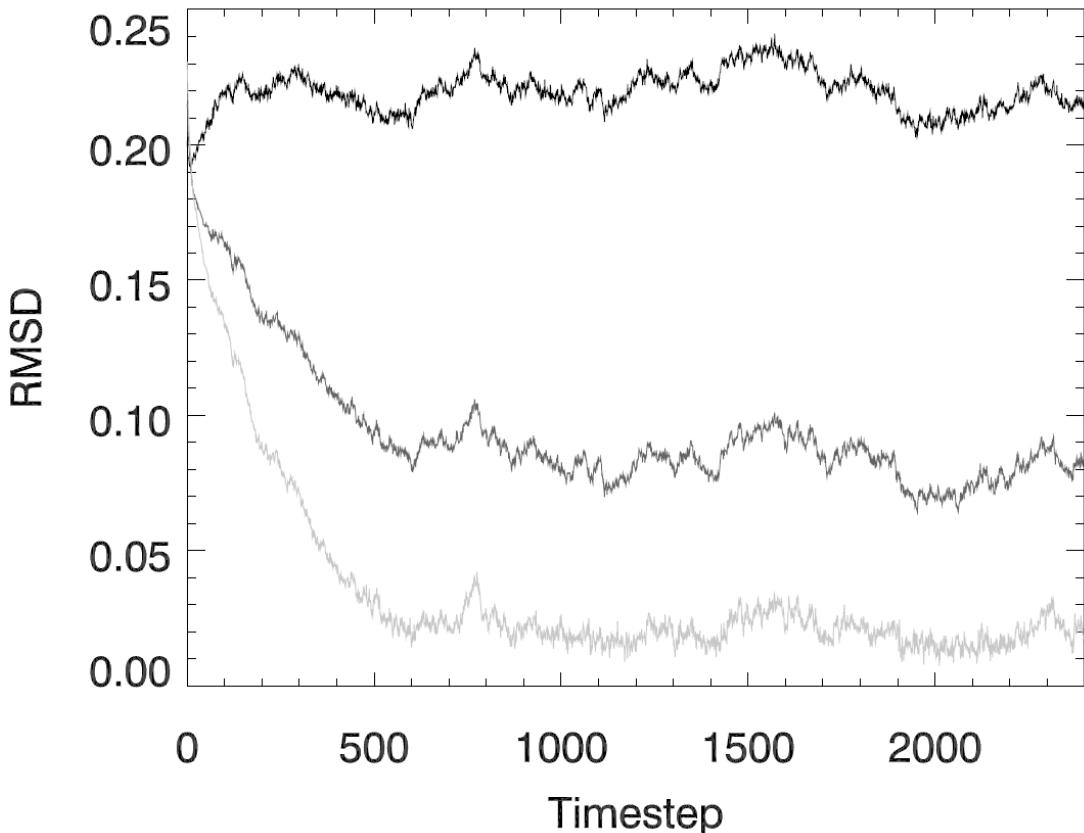
$$261 \quad C = e^{\frac{-w_s z}{k_z}} \quad (11)$$

262 As shown in Figure 3, the model properly simulates the change in concentration due to vertical
 263 settling and mixing while allows the particles to remain approximately uniformly distributed in the
 264 vertical. The simulation accuracy increases with increased resolution of vertical layers. The model
 265 result with 20 vertical layers shows a close agreement with the analytical solution. Specifically, Figure
 266 4 shows the evolution in time of the root mean square difference (RMSD) between the cell averages
 267 and the analytical solution for the three cases. While the RMSD in the simulation with 5 layers
 268 remains above 0.2 (the magnitude of initial error) over the entire simulation, the RMSD decrease
 269 quickly to 0.02 after 500 time steps and stay stable at such level when vertical resolution increases to
 270 20 layers.



271

272 **Figure 3.** The PCPM simulation of vertical settling in comparison to the analytical solution at the end
 273 of 5,000 time steps. Three runs were made with 5, 10, and 20 vertical cells, respectively. The dots
 274 represent the locations of the particles on the vertical axis with their respective concentration on the
 275 horizontal axis. The thin line represents the cell average concentration and the thick line represents
 276 the analytical solution.



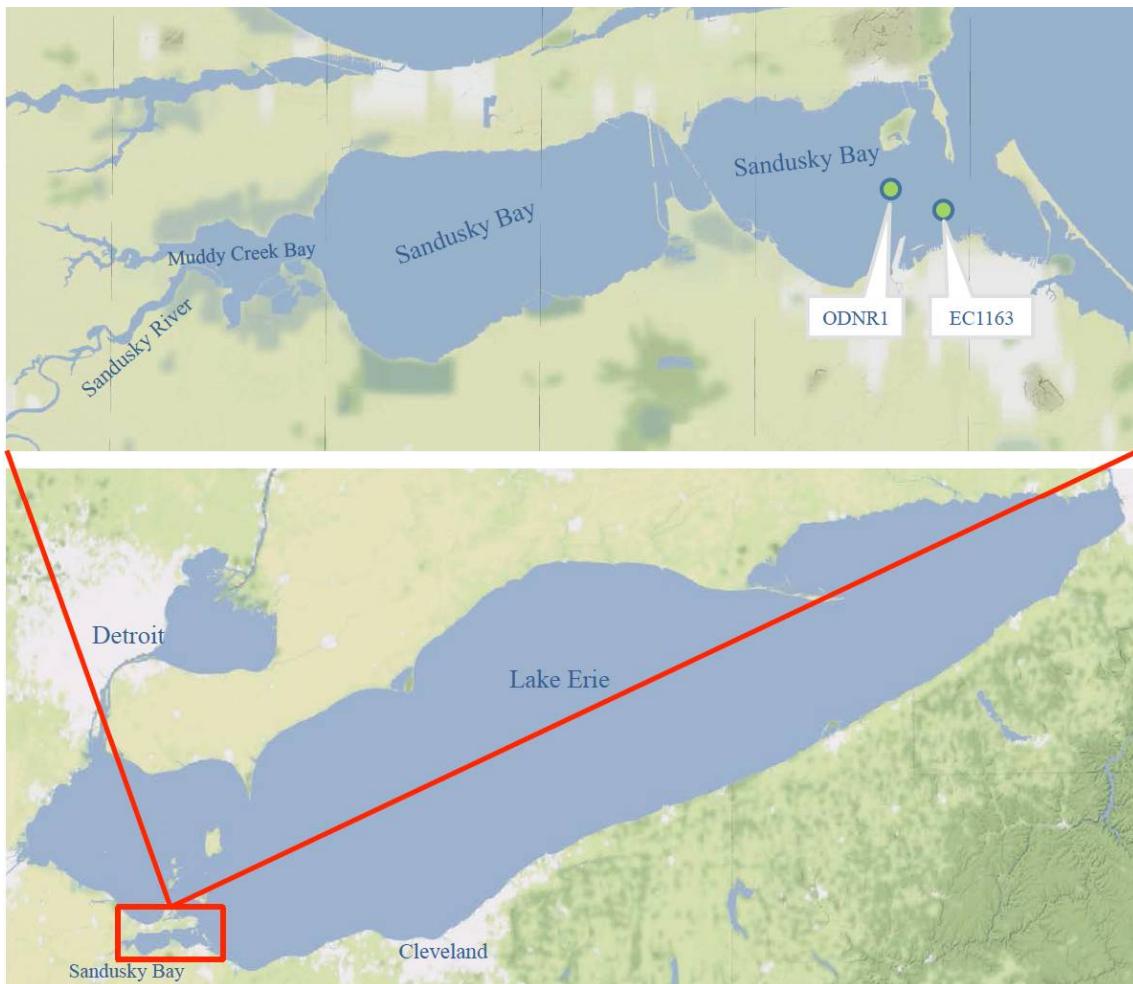
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278 **Figure 4.** The time evolution of the root mean square difference (RMSD) between the cell averages
279 and the analytical solution for the three cases presented in the Figure 3 (dark line for 5 cells, medium
280 line for 10 cells, and light line for 20 cells).

281 **4. Application to Sandusky Bay**

282 To illustrate more clearly the type of application envisioned for PCPM, we constructed and
283 applied a rudimentary biophysical model to an actual aquatic system, Sandusky Bay. Since the mid-
284 1990s, harmful algal blooms (HABs) have become the new norm for summer months in the Lake Erie
285 ecosystem [11]. Harmful algal blooms occur in the system when cyanobacteria are provided the right
286 temperature, light, and nutrient conditions to proliferate. When these blooms transpire, they have
287 many adverse impacts. At the local ecosystem level, HABs result in depleted dissolved oxygen levels
288 below the lake's surface threatening the survival of organisms living below the surface. Additionally,
289 some cyanobacteria species produce a toxin, such as microcystin, which affects the nervous system,
290 liver, and kidney further impeding aquatic organisms and humans.

291 Situated on Lake Erie's southwestern coast is the focus of this study, Sandusky Bay (Fig. 5).
292 Sandusky Bay borders Ohio's Ottawa, Erie, and Sandusky counties. Each of which relies heavily on
293 Sandusky Bay. From a physical aspect, Sandusky Bay is relatively shallow bay with an average depth
294 of roughly 2.6 meters as well as occupying a relatively small area [12]. The primary draining
295 watershed to Sandusky Bay originates from the Sandusky River on the west end of the bay. The
296 Sandusky River drains a 1,420 square mile area; of which, over 80% is dedicated to agricultural
297 production [11]. This largely agricultural watershed leads to high nitrogen and phosphorus entering
298 Sandusky Bay. Combining these high nutrient loads with the physical aspects leads to very high
299 concentrations of nitrogen and phosphorus within Sandusky Bay, thus resulting in these
300 cyanobacteria blooms (*Planktothrix agardhii*) [12,13].



301

302 **Figure 5.** Sandusky Bay is situated on Lake Erie's southwest coast occupying a small portion of the
303 Great Lake's coastline. Sandusky Bay is relatively shallow bay with an average depth of ~2.6 meters.
304 The primary draining watershed to Sandusky Bay originates from the Sandusky River on the west
305 end of the bay. Sampling stations ODNR1 and EC1163 are denoted with green dots.

306 In this study, the intent of the work is to test the PCPM feasibility for biological-physical coupled
307 model by implementing it in relation to HABs in Sandusky Bay. The physical model utilizes the 3-D
308 Finite Volume Community Ocean Model (FVCOM) based on an unstructured grid. The biological
309 model is a 1-D NPZD model.

310 *4.1. Observational Data*

311 To aid in model development, several datasets are gathered from literature as well as data
312 acquisition organizations. Sandusky river daily discharge and nitrogen concentration are available
313 from National Center for Water Quality Research (<https://ncwqr.org/monitoring/data/>). Nitrogen,
314 Chlorophyll concentration, and in-situ temperature data are available from two observational sites
315 (ODNR1 and EC1163) in the eastern bay from May – October 2015, sampled by Bowling Green State
316 University [13].

317 *4.2. Hydrodynamic Model*

318 The hydrodynamic model used in this study is FVCOM (Finite Volume Community Ocean
319 Model) [14]. FVCOM is an unstructured-grid, finite-volume, three-dimensional (3-D) primitive
320 equation ocean model with a generalized, terrain-following coordinate system in the vertical and a
321 triangular mesh in the horizontal. The unstructured grid can be designed to provide a customized
322 variable resolution to both coastline and bathymetry. With the merits of ideal geometric fitting and

323 local refinement of mesh resolution, FVCOM has been used in numerous applications to estuaries,
324 coastal oceans, and the Great Lakes [16-20]. These characteristics make the model well suited for the
325 study of Sandusky Bay.

326 Although this study focuses on Sandusky Bay, FVCOM is configured to simulate physical
327 dynamics for all of Lake Erie, thus providing reliable representation of large scale background
328 circulation and the role of remote forcing impacting the water movement in the bay through the
329 opening; additionally, this configuration avoids the impact of setting an artificial numerical boundary
330 condition for our target region. The hydrodynamic model is well-calibrated for the Lake Erie, based
331 on the next-generation NOAA Lake Erie Operational Forecast System [LEOFS; see Kelley et al., [21]
332 for detailed model validation], a real-time nowcast and forecast model that is built on the FVCOM.
333 In the upgraded NOAA operational model for Lake Erie [21], the FVCOM model is developed with
334 horizontal resolution ranging from 100 to 2500 meters, and 21 uniform vertical sigma (terrain-
335 following) layers for Lake Erie. The advantage of our model setting is that model resolution varies
336 from 100-2500 m (coarse) in the open lake to 10-50 m (fine) in Sandusky Bay, affording a high degree
337 of resolution across the 20 km x 3 km study site and adequately resolving the geographic complexity
338 and coastal hydrodynamic conditions of that system (Figure 6). The model configuration yields a
339 total of 73,000 grid elements (cells) in the horizontal plane with 50,000 of them resolving the bay.



340

341 **Figure 6.** FVCOM model mesh for Lake Erie (upper panel) and linked with a high-resolution mesh
342 for Sandusky Bay (lower panel). Only a portion of the Sandusky Bay mesh is displayed for a clear
343 representation of the mesh's resolution.

344 4.3. Biological Model

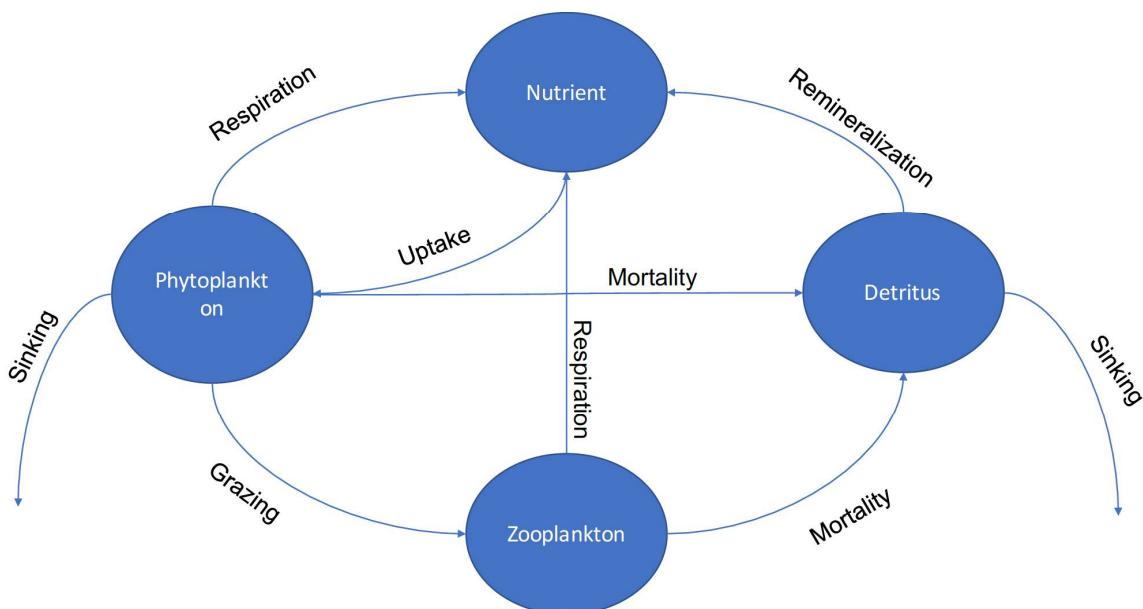
345 The biological model used in this work is a general 1-D NPZD model. The governing equations
 346 for the model framework are based on Luo et al. [22]. Figure 7 displays the interactions among state
 347 variables in the NPZD model.

348
$$\frac{dN}{dt} = -P(\text{uptake}) + Z(\text{respiration}) + P(\text{respiration}) + D(\text{remineralization}) + N(\text{mixing})$$

349
$$\frac{dP}{dt} = P(\text{uptake}) - P(\text{respiration}) - P(\text{mortality}) - ZP(\text{grazing}) + P(\text{mixing})$$

350
$$\frac{dZ}{dt} = ZP(\text{grazing}) + ZD(\text{grazing}) - Z(\text{respiration}) - Z(\text{mortality}) + Z(\text{mixing})$$

351
$$\frac{dD}{dt} = P(\text{mortality}) + Z(\text{mortality}) - ZD(\text{grazing}) - D(\text{remineralization}) + D(\text{mixing})$$



352

353 **Fig. 7.** A schematic representation of the NPZD model.

354 Several equations in the governing equations are modified for this study based on literature
 355 review. The light-limited, nutrient-limited, and temperature-limited functions ($f(I)$, $f(N)$, $f(T)$),
 356 respectively, that contribute to the $P(\text{uptake})$ are taken from Platt et al. [23] and Nicklisch et al. [24].
 357 Also, the light attenuation functions are adjusted to Rowe et al. [25].

358
$$f(I) = (1 - e^{-\frac{\alpha_I I}{\mu_{max}}})e^{-\frac{\beta_I I}{\mu_{max}}} \quad (12)$$

359
$$f(N) = \frac{N - N_0}{K_s + N - N_0} \quad (13)$$

360
$$f(T) = \exp(-2.3(\frac{T_{opt} - T}{T_{opt} - T_{min}})^2) \quad (14)$$

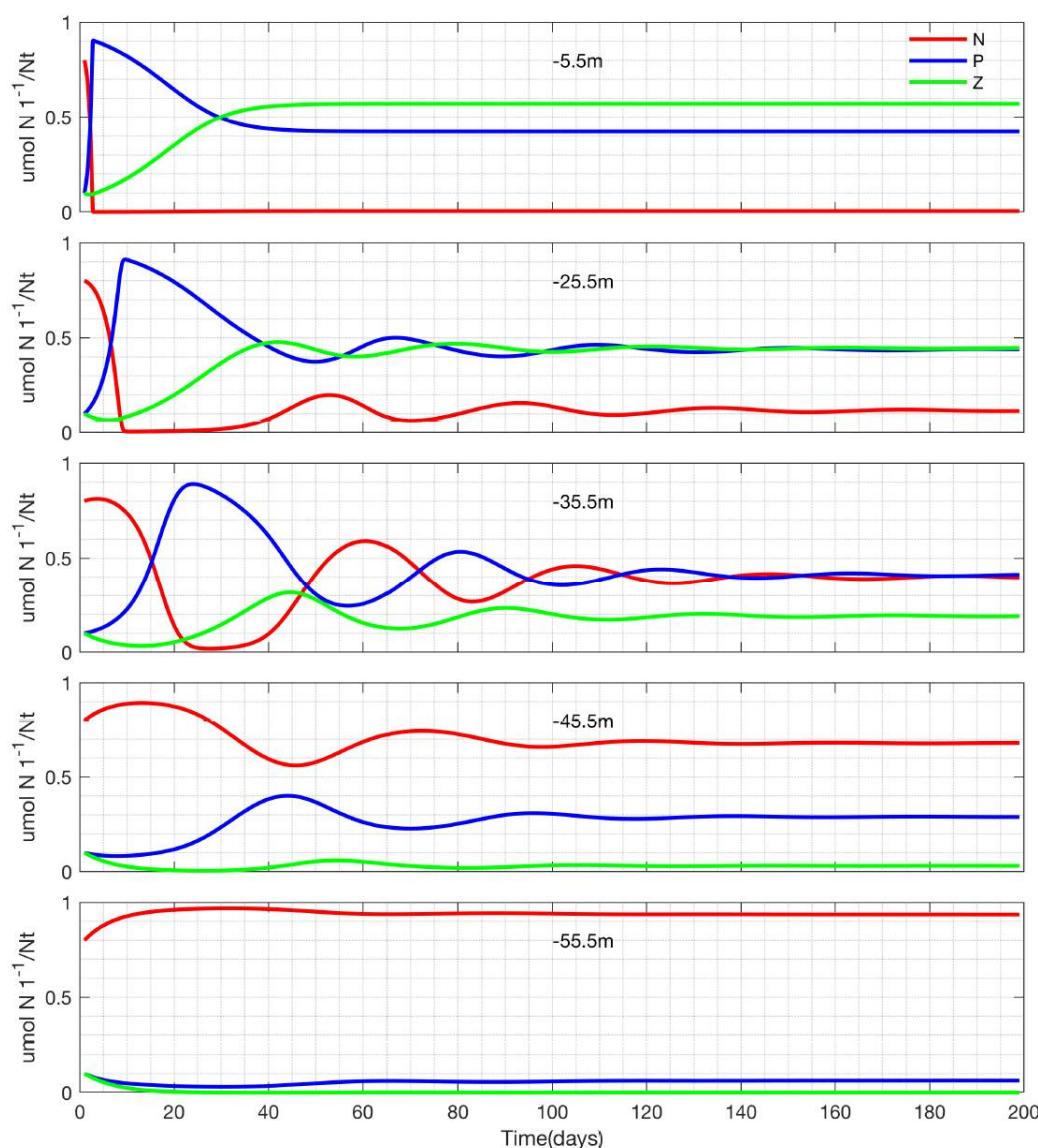
361
$$I = I_0 \exp(-k_d h) \quad (15)$$

362

363 where α_I , β_I are the initial linear slope at low irradiance and the negative slope at the high irradiance
 364 that characterizes photoinhibition [26], μ_{max} is the maximum potential growth rate, and I is the light
 365 intensity. The nutrient threshold N_0 represents the pool of nutrient that was assumed to be
 366 biologically unavailable. T_{opt} and T_{min} are the optimal growth temperature and minimal growth
 367 temperature, respectively. k_d is the light attenuation coefficient that accounts for the impact of

368 water turbidity, phytoplankton, and detritus on the light attenuation. Model parameterization is
 369 based on literature review [22,24-26] and subjective tuning for the Sandusky Bay simulation.

370 To ensure validity of the 1-D NPZD biological model, several scenarios from Edwards et al. [27]
 371 are reproduced with the same model configuration. As an example, Figure 8 demonstrates the linear
 372 stability of a vertically-distributed, NPZ ecosystem model and the impact of vertical mixing on
 373 biological dynamics. The nutrient-phytoplankton-zooplankton concentrations in terms of nitrogen
 374 ($\mu\text{mol N L}^{-1}$) at different depths are displayed in the water column. In the surface waters, it reaches
 375 equilibrium values. Notice in the second panel (depth = 25.5 m), oscillations develop in the curves
 376 indicating the model's instability below this depth. Under linear stability analysis, this incidence can
 377 be discerned from the fact that the eigenvalues have a real part [27]. However, at unstable mid-depths
 378 the fields return to equilibrium, as a damped oscillator due to vertical mixing, consistent with
 379 complex eigenvalues from linear stability analysis [27].

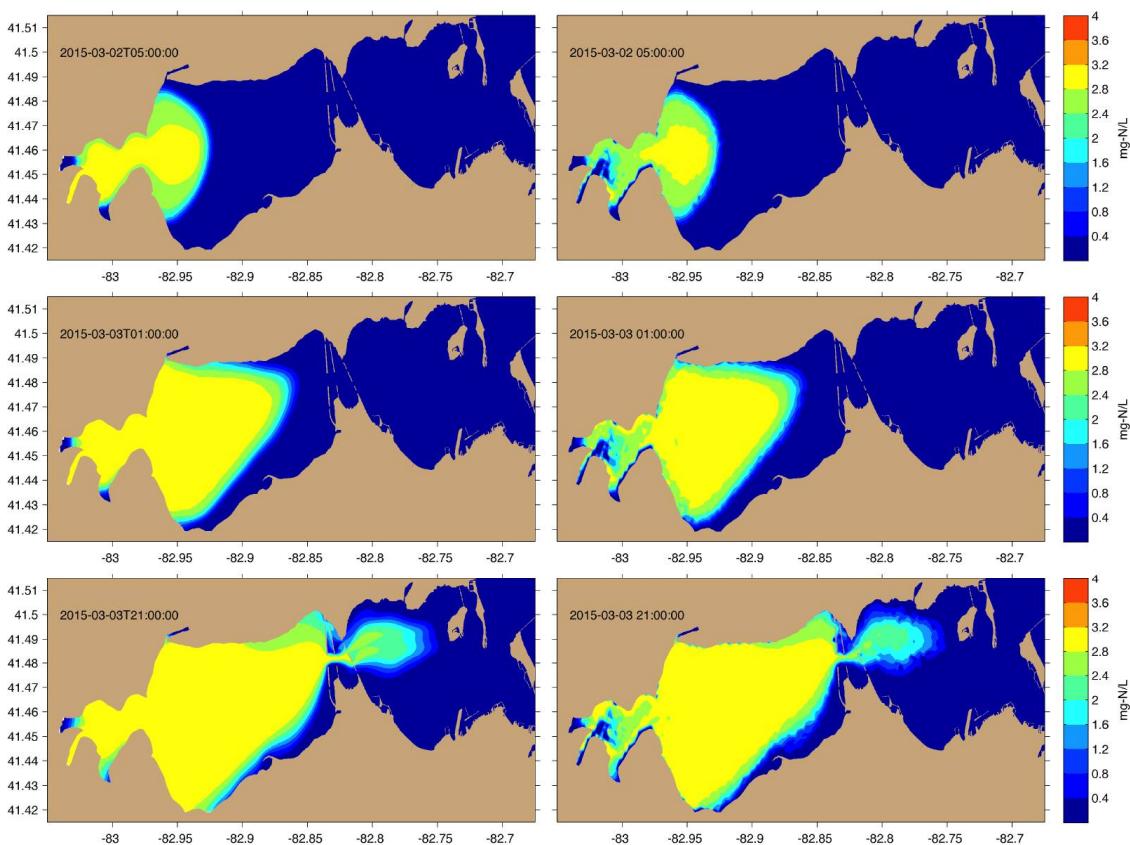


380

381 **Figure 8.** Reproduced scenarios using our NPZD model from Figure 6 in Edwards et al. [27] as a
 382 biological model verification, in which detritus is not considered. Time series solution of the diffusive
 383 NPZ model at depths (a) 5 m, (b) 25 m, (c) 35 m, (d) 45 m, and (e) 55 m. Notice that in the water layer
 384 below 25.5 m, there are damped oscillations over time, consistent with the linear stability analysis
 385 showing complex eigenvalues with negative real parts below 25.5m. See detailed discussion in the
 386 linear stability analysis in Edwards et al. [27].

387 **4.4 Results**

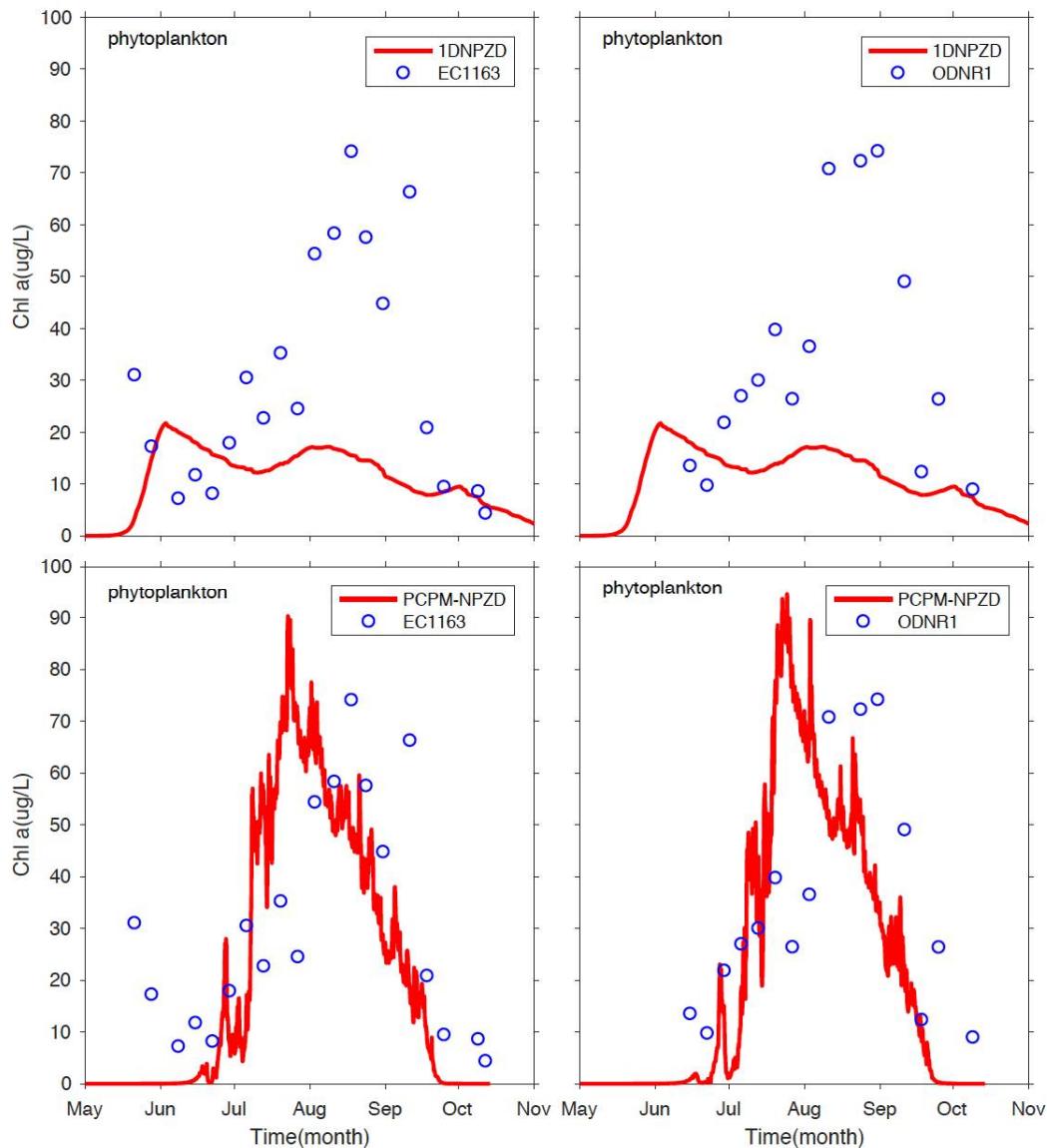
388 Before examining the impact of physical transport on the biological dynamics, we first validate
 389 the representation of advection-diffusion in PCPM. The river plume is simulated using the
 390 conventional soluble-tracer model based on Equation 1 and PCPM model for plume modeling (Fig.
 391 9). It is clear that the plumes simulated using the two methods show a very similar pattern,
 392 indicating the validity of the PCPM. Upon closer review, the plume simulated with soluble-tracer
 393 model shows a smoother evolution near the plume front, and a better representation of plume in
 394 Muddy Creek Bay in comparison to the PCPM. This indicates denser particles release may be needed
 395 in the mouth of the Sandusky River. Nonetheless, the attractiveness of PCPM is its computation
 396 efficiency; it runs ~100 times faster than the soluble-tracer model which will be discussed in detail in
 397 the following section.



398

399 **Figure 9.** River plumes simulated with conventional soluble-tracer model (left panels) and PCPM
 400 model (right panels). The color scale represents the nitrogen concentration.

401 Using the PCPM-NPZD model, the importance of physical transport is demonstrated by
 402 comparing model results between the NPZD standalone simulation and PCPM-NPZD simulation.
 403 The comparison of model results is presented in Figure 10. The simulation using NPZD standalone
 404 model without resolving the transport processes shows a large discrepancy from observational data
 405 (Fig. 10, upper panels). The model completely fails to capture both the timing and magnitude of the
 406 blooms. On the other hand, after the impact of advective processes is resolved using PCPM, the model
 407 accurately depicts the magnitude of the chlorophyll peak in mid-August. Although further
 408 development of the NPZD is certainly necessary to resolve the onset and variability of the algal
 409 blooms, it is beyond the scope of this work, which focuses on demonstrating the feasibility of linking
 410 hydrodynamic effects and biological processes through the PCPM in a Lagrangian/Eulerian
 411 framework. The further development of the biological model and its application to the mechanisms
 412 study for the HABs in Sandusky Bay will be presented in a companying paper.



413

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415

416

Figure 10. Observed (blue dots) and model simulated (red lines) Chlorophyll concentration at the sampling stations EC1163 and ODNR1. The upper panels are results from the standalone 1-D NPZD model simulation; the lower panel are the results from the coupled PCPM-NPZD model simulation.

417

5. Summary and Conclusions

418

In this paper, we describe a novel method by integrating a property-carrying particle model (PCPM) and an Eulerian concentration biological model for ecosystem modeling. The model is tested in idealized cases and its utility is demonstrated in a practical application to Sandusky Bay. The novelty of this new technique lies in its integration of hydrodynamic effects via the property-carrying particle tracking model and Eulerian grid-based biological modeling approach. Overall, there are several advantages of the PCPM over traditional Eulerian-based tracer approaches. The PCPM is simpler to implement and more efficient as it does not need to solve the advection-diffusion equation. Instead, the PCPM uses pre-computed particle trajectories to resolve the hydrodynamic condition based on currents from a hydrodynamic model. This means that the hydrodynamic model only needs to be run once giving one the ability to run different biological scenarios for the same physical characteristics; ultimately saving significant computational time.

429

For example, 1-year hydrodynamic simulation with the particle tracking model in Sandusky Bay case takes 5 day to complete using 64 CPUs. Once the hydrodynamic simulation is done, the PCPM can complete its 1-year river plume simulation using the particle trajectories as input within 10

430

431

432 minutes using a single CPU while it takes 12 hours for soluble-tracer model to complete the same
433 simulation using 32 CPUs. In the PCPM framework, the hydrodynamics and associated water
434 transport and mixing represented by particle trajectories are “reserved” and not affected by
435 biochemical properties. In other words, it only takes another 10 minutes to run the PCPM for a
436 different set of parameters and property configurations. This is extremely useful during the model
437 calibration and or ensemble simulations. Such a high level of efficiency is not available from tracer-
438 based models because one will have to re-run the soluble-tracer model for any change in parameter
439 configuration or estimation of different property concentration. In addition, the PCPM is capable of
440 providing comparable simulation results to the soluble-tracer model, although the global and local
441 mass conservation is not strictly preserved with finite particles. Above all, it is the PCPM’s
442 computational efficiency and coupling flexibility which makes it an attractive alternative method to
443 the traditional approach.

444

445 **Author Contributions:** Conceptualization, Pengfei Xue and David Schwab; Formal analysis, Xing Zhou, Chenfu
446 Huang and Xinyu Ye; Project administration, Pengfei Xue; Validation, Xing Zhou; Visualization, Xing Zhou,
447 Chenfu Huang and Xinyu Ye; Writing – original draft, Pengfei Xue and David Schwab; Writing – review &
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454

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