

## Article

# Integrable Near-Infrared Photodetectors Based on Hybrid Erbium/Silicon Junctions

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**Abstract:** This paper presents the design, fabrication and characterization of Schottky erbium/silicon photodetectors working at 1.55  $\mu$ m. These erbium/silicon junctions are carefully characterized using both electric and optical measurements at room temperature. A Schottky barrier  $\Phi_B$  of ~673 meV is extrapolated; the photodetectors show external responsivity of 0.55 mA/W at room temperature under a 8 V of reverse bias applied. In addition, the device performance is discussed in terms of normalized noise and noise equivalent power. To the best of our knowledge, these are the first Er/Si photodetectors designed for operation in free space at 1.55  $\mu$ m. The proposed devices will pave the way towards development of Er-based photodetectors and light sources to be monolithically integrated in the same silicon substrate and both operating at 1.55  $\mu$ m.

**Keywords:** silicon; near-infrared; photodetectors, internal photoemission; erbium.

## 1. Introduction

The integrated photonics refers to the fabrication and integration of several photonic components on the same planar substrate. These components include beam splitters, gratings, couplers, polarizers, interferometers, sources and detectors, among others. In the last three decades, there has been growing interest in the use of silicon (Si) as substrate for integrated photonics [1]. In this context, tremendous progresses in the technological processes based on the use of silicon-on-insulator (SOI) substrates have allowed to obtain reliable and effectiveness optical components fully compatible with the complementary metal-oxide semiconductor (CMOS) technology, such as: low loss waveguides, high-Q resonators, high speed modulators and couplers, typically operating at near-infrared wavelengths [2-7].

However, the silicon indirect band-gap and the minimal optical absorption at NIR wavelengths limit the use of Si for some active optical components like sources (led, laser) or NIR photodetectors (PDs).

The latter issue is typically addressed by the integration with Germanium (Ge). Unfortunately, the growth of Ge on a Si substrate is only achievable with a two-step epitaxial growth technique [8, 9] that causes problems in both thermal budget and planarity [10] hindering the monolithically integration of an electronic and photonic circuitry on the same Si substrate. Indeed, Intel [11] and Luxtera [12] reported on four-channel optical receiver working at 50 Gbps and 40 Gbps, respectively, based on Ge PDs that are separately fabricated and only subsequently flip-chip mounted to a Si electronic circuitry. In addition, there has been progress in fabricating SiGe-based PDs in such a 'zero-change' CMOS process flow [13], but the Ge content of the available layer is estimated to be 25% to 35% [14] and consequently the wavelength of possible detection is limited to less than 1200 nm [15]. A single-chip microprocessor integrating over 70 million transistors and 850 photonic components has been fabricated taking advantage of SiGe PDs fabricated by a 'zero-change' CMOS approach operating at 1180 nm [16]. Unfortunately, no Ge-based PDs operating at 1550 nm has been realized by a 'zero change' approach as far.

Thanks to the success of the so-called EDFA (Erbium-doped fiber amplifier) used in telecommunications, in the last years many efforts have been aimed to introduce Er in Si in order to realize Si-based light sources. Unfortunately Si is not a good host for Er. The reason is believed to be linked to a back-transfer process of energy that strongly reduces the light emission at room temperature. The attractive features of this technology are the emission in the telecommunications band of 1550 nm as well as the electrical pumping. For this aim, metal-oxide-semiconductor (MOS) structures are typically realized: a voltage applied between metal and Si causes electrons to tunnel through the oxide in which Er ions are dispersed, exciting them. In a subsequent version of the device Si nanocrystals are dispersed together Er ions in the oxide. Light emitting diodes based on this approach show efficiencies of about 10% as reported by STMicroelectronics [17] even if the light emission is observed to diminish when the current density increases. This effect is believed to be due to free carrier absorption and Auger processes, thus, despite of first preliminary successes, many concerns need still to be addressed.

Although Erbium results a very promising material for the realization of Si-based LASER, no investigations have been performed on the use of hybrid Er/Si structures in the field of the near-infrared detection. Indeed, this could be very fascinating in the vision of integrating both Er-based LASER and PDs on the same silicon substrate. In addition, Er can be deposited by sputtering at low temperature without compromising an eventually pre-existent electronic circuitry. On the other hand, sputtered Er deposited on Si has already shown the capability to form Schottky junctions [18] that have been widely employed in both infrared and NIR detection [19-23].

In this work we report on Er-based Schottky PDs operating at 1550nm and integrated with a double-polished 200 $\mu$ m-thick Si substrate. Er has been deposited by a radio-frequency (RF) sputtering process at low temperature and its optical properties have carefully been characterized by ellipsometric techniques. The photocurrent generation is based on the internal photoemission effect, where photoexcited carriers from Er are emitted into Si over the Schottky barrier  $\Phi_{B0}$ . The rectifying Schottky diode behavior is shown from the IV curve, from which both the series resistance and the ideality coefficients are extrapolated together with a Schottky barrier  $\Phi_{B0}$  of  $\sim$ 673 meV. We show that an external responsivity (photogenerated current-incident optical power ratio) of  $R_{ext} \sim 0.29$  mA/W at 1V reverse bias, can be obtained; this value increases up to  $\sim$ 0.55 mA/W when a reverse voltage of 8V is applied. We believe that this work paves the way to the realization of microsystems where Er-based sources and photodetectors are monolithically integrated on the same Si substrate.

## 2. Materials and Methods

### 2.1 Erbium deposition

A Radio-Frequency (RF) Sputtering technique was used for depositing the Erbium (Er) thin film directly on the Si substrate, from a 99,9% pure metal Er target. The substrate was placed on the holder and the deposition chamber was pumped down to a base pressure of  $3 \cdot 10^{-6}$  mbar before introducing the process gas (Ar). Er film was then deposited at r.t., with 30 W RF power, at  $2.5 \cdot 10^{-2}$  mbar pressure, with a constant 40 sccm Ar flux and 11 min deposition time. To overcome the target surface oxidation a 30 min presputtering process at 150 W RF power was necessary before the deposition process.

### 2.2 Erbium ellipsometric characterization

Spectroscopic ellipsometry data were recorded using a phase modulated spectroscopic ellipsometer (UVSEL, Jobin Yvon Horiba) with a wavelength scanning range from 300 to 1600 nm, at an incident angle of 70°. Acquired data were fit to an optical model of the sample in which the dispersion of the erbium film was assumed to follow a classical dispersion model [24, 25] based on the sum of the single and double Lorentz, and Drude oscillators:

$$\tilde{\varepsilon}(\omega) = \varepsilon_{\infty} + \frac{(\varepsilon_s - \varepsilon_{\infty}) \cdot \omega_t^2}{\omega_t^2 - \omega^2 + j\Gamma_0 \cdot \omega} + \frac{\omega_p^2}{-\omega^2 + j\Gamma_d \cdot \omega} + \sum_{i=1}^2 \frac{f_i \cdot \omega_{0i}^2}{\omega_{0i}^2 - \omega^2 + j\gamma_i \cdot \omega} \quad (1)$$

The Lorentz oscillator model works well for insulators and semiconductors above the band gap, while the Drude model describes well the optical properties of metals but does not take into account the notion of optical band gap energy  $E_g$ . The combination of both is often adequate when the material is a little conductive and has a metallic character. In our case, for the erbium dielectric function assessment, was introduced only one of the two oscillators of the last term. Fitting of experimental data leads to film thickness and dielectric function  $\tilde{\epsilon} = \epsilon_1 - j\epsilon_2$  evaluation; the complex refractive index come from the dielectric function assuming that  $\tilde{\epsilon} = n^2 = (n - jk)^2$ . The film structure used in the model consists of a homogeneous bulk erbium film and an outmost layer, described by a Bruggeman effective medium approximation (BEMA) [26].

### 2.3 Electrical characterization

To electrically characterize the PD, we measure the current-voltage (I-V) characteristics of the Er/p-Si Schottky junction when p-Si is biased with respect to grounded Er electrode. The I-V characteristics were acquired using a Keithley 6487 picoammeter. Fig. 3a is the mean of five curves that were obtained by varying the voltages repetitively from -8 V to 2 V and vice-versa.

### 2.3 Optoelectronic characterization

For optoelectronic characterization, a tunable NIR laser (AQ4321D, Ando) was collimated, chopped and split into two beams using a beam splitter. One beam was focused by a  $20\times$  IR microscope objective (MO) to the device under test (DUT). The transmitted light was collected using a  $20\times$  IR collecting MO and addressed on a NIR CCD to simplify the alignment procedure. A lock-in amplifier was used to measure the photocurrent produced by the DUT. The second beam was sent to a calibrated commercial power meter to perform incident optical power measurements and, consequently, to calculate the external responsivity.

## 3. Results and discussion

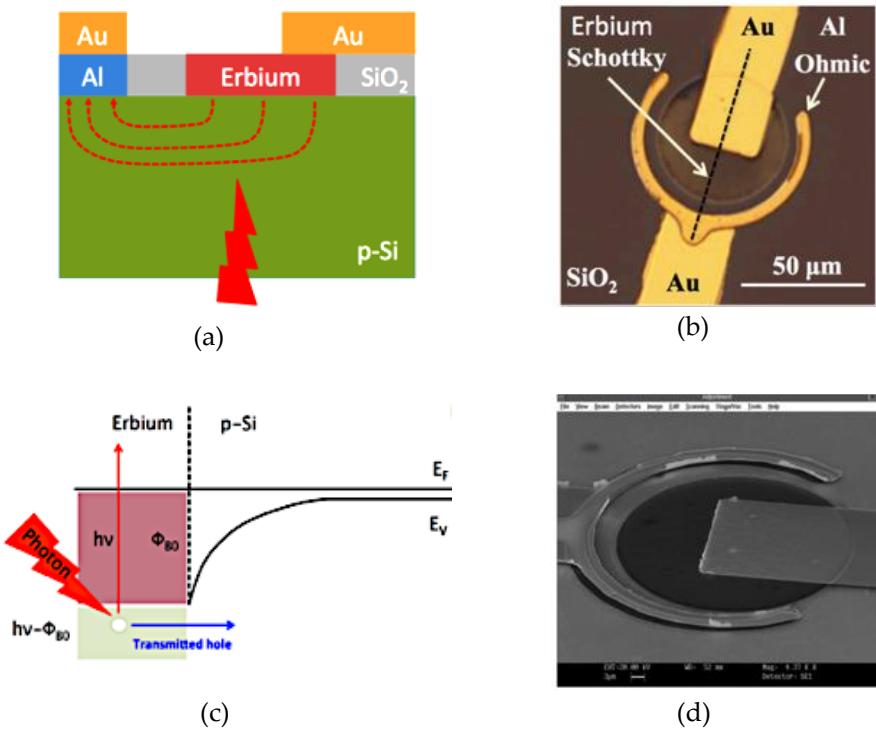
### 3.1. Fabrication and theoretical background

Devices reported in Figure 1 have been fabricated starting from a bi-polished 200- $\mu\text{m}$ -thick very lightly doped P silicon. Substrate was chosen slightly doped in order to avoid free carrier absorption.

After a RCA Si cleaning process, the Si substrate has been thermally oxidized in order to obtain a 100-nm-thick silicon dioxide ( $\text{SiO}_2$ ). The two electrodes, the collecting Ohmic contact and the Schottky contact, were both realized on the top of the substrate. The collecting contact was made by a ring of 200-nm-thick aluminium film, thermally evaporated at  $3 \times 10^{-6}$  mbar and 150 °C.

First of all the Shipley S1813 photoresist (PR) was deposited by spin coating at 4000 rpm, by resulting in a PR thickness of 1.4  $\mu\text{m}$  and then a standard photolithography process was used to form a ring pattern. After that a  $\text{SiO}_2$  wet etching process was performed and, after the aluminium thermal evaporation, a lift-off process was carried out in order to obtain a directly contact between Al and Si. Then an annealing at 475 °C in nitrogen for 30 min, to get a not-rectifying behaviour, was carried out.

The Schottky contact was fabricated by sputtering deposition of 50 nm thick erbium film. The top of the wafer was covered by Shipley S1813 PR, exposed and developed in order to obtain a disk surrounded by the Al ring Ohmic contact.



**Figure 1.** (a) Schematic cross-sectional view of the graphene/Si Schottky PD under illumination; (b) optical image of a sample device; (c) the IPE mechanism in a Er/p-Si Schottky junction, where  $E_F$  is the Fermi energy of the metal,  $E_V$  is the Si valence band energy and  $h\nu - \Phi_B$  is the difference between the photon energy and the Schottky barrier; (d) SEM image of the device.

Then the Ebium active materials was deposited as reported in the Section 2 and subsequently patterned. Finally, two gold (Au) electrodes have been realized, by standard photolithography and lift-off process, in order to connect both Schottky (Er) and Ohmic (Al) contact of the device to the macroscopic world.

Internal quantum efficiency of Si-based Schottky PDs can be written as  $\eta_{int} = C \cdot \frac{(h\nu - \Phi_B)^2}{h\nu}$  [27, 28], where  $C$  is the quantum efficiency coefficient,  $h\nu$  is the energy photon and  $\Phi_B$  is the Schottky barrier height (SBH). On the other hand,  $\eta_{int}$  is linked to the external responsivity  $\eta_{ext} = A \cdot \eta_{int}$ , where  $A$  is the metal absorption can be written as:

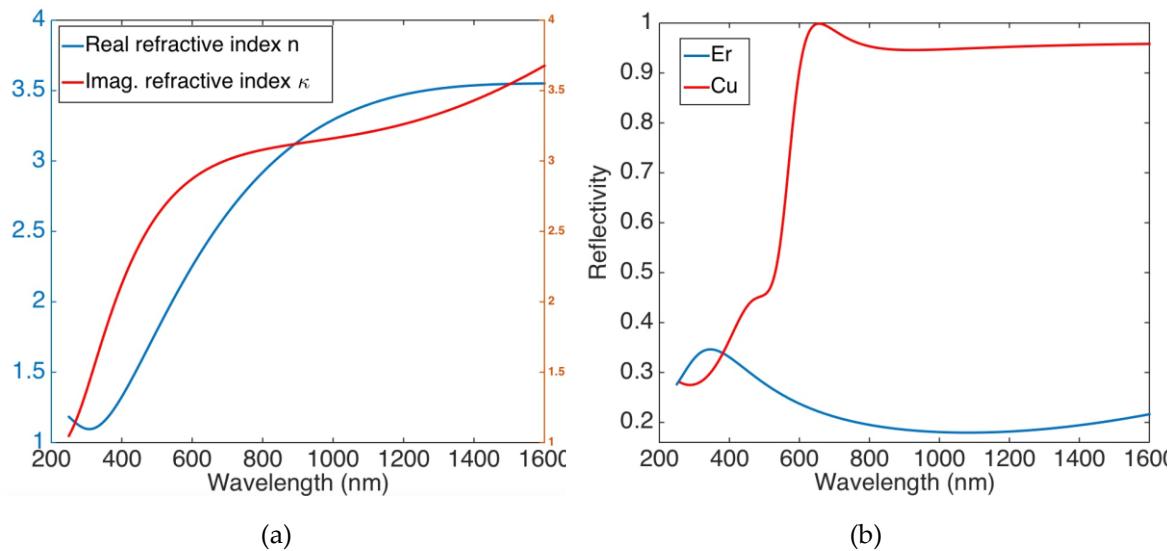
$$A = (1 - R) \cdot (1 - e^{-\alpha \cdot d}) \quad (2)$$

where  $R$  is the reflectivity at the metal/Si interface,  $\alpha$  and  $d$  are the absorption coefficient and thickness of the metal, respectively. The absorption coefficient  $\alpha$  is linked to the penetration depth  $\delta = 1/\alpha$ , thus in the limit of metal thickness  $d \gg \delta$ , all optical power going in the metal will be absorbed and  $A = 1 - R$ . This means that the lower the reflectivity the higher the absorption (and the higher the efficiency). The corresponding external responsivity can be written as [26]:

$$R_{ext} = \frac{q}{h\nu} \cdot \eta_{ext} = (1 - R) \cdot C \cdot \frac{(h\nu - \Phi_B)^2}{h\nu^2} \quad \left[ \frac{A}{W} \right] \quad (3)$$

### 3.2. Erbium Characterization

Figure 2 shows the ellipsometric characterization carried out on the sputtered Er in term of complex refractive index and reflectivity.

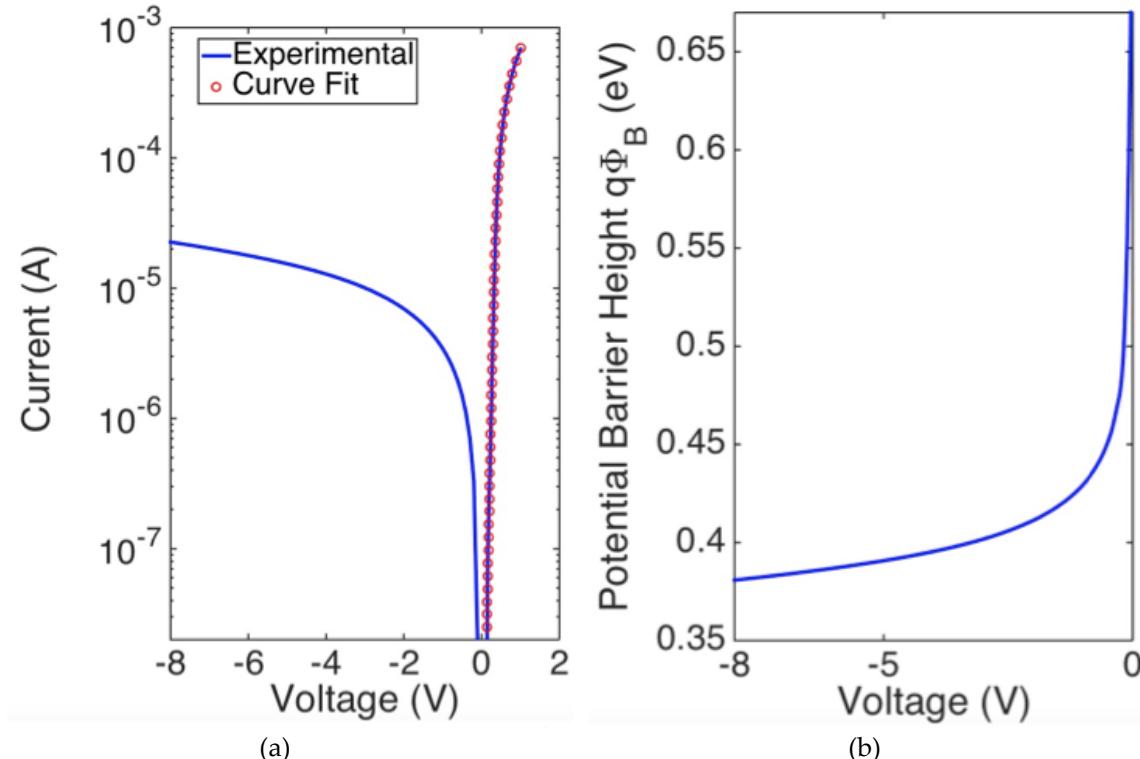


**Figure 2.** (a) real (blue) and imaginary (red) refractive index of sputtered Er measured by ellipsometric characterization; (b) Simulated reflectivity at both Si/Cu and Si/Er interface for normal incidence.

Figure 2(a) shows that Er is characterized by a extinction coefficient of  $\kappa=3.68$  at  $\lambda_0=1550$  nm; it leads to an absorption coefficient ( $\alpha=4\pi\kappa/\lambda_0$ ) and penetration depth ( $\delta=1/\alpha$ ) of  $29.8 \mu\text{m}^{-1}$  and  $33.6 \text{ nm}$  at 1550 nm, respectively. By using the Fresnel coefficient for normal incidence the reflectivity of the Si/Er interface is reported in Figure 2(b) where the reflectivity of Si/Cu interface is reported for comparison, too.

### 3.3. Electrical characterzation

Fig. 3(a) shows the I-V experimental characteristics of the Er/p-Si Schottky junction.



**Figure 3.** (a) I-V characteristics of Er/p-Si PD at room temperature; (b) Potential barrier height as a function of reverse bias.

The device shows rectifying I-V diode behavior, which follows the Schottky diode equation [29]:

$$I = I_S \cdot \left( e^{\frac{q(V-R_s I)}{\eta k_B T}} - 1 \right) \quad (4)$$

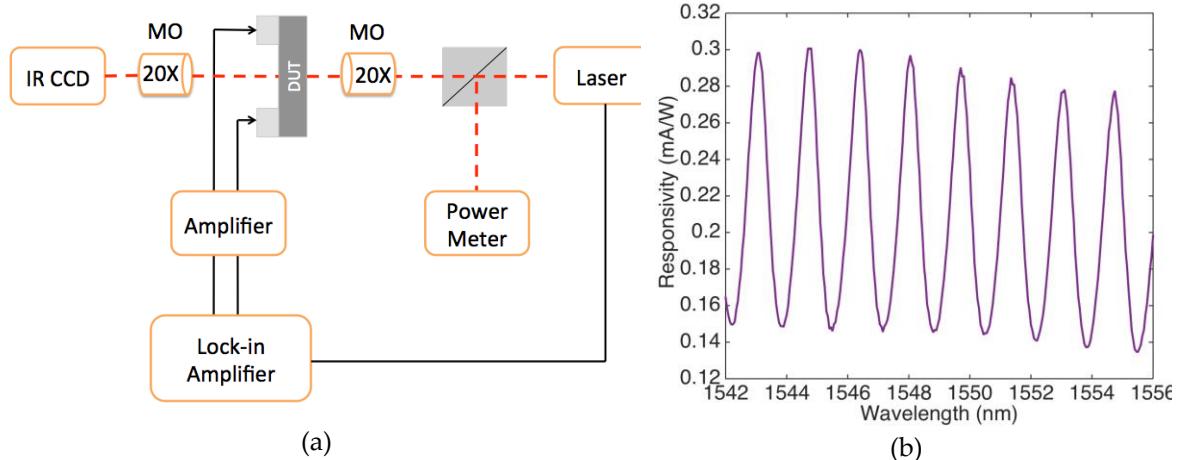
$$I_S = A A^* T^2 e^{-\frac{q \Phi_B}{k_B T}} \quad (5)$$

where  $\Phi_B(V) = \Phi_{B0} - \Delta\Phi(V)$ ,  $\Phi_{B0}$  is the SBH at zero voltage,  $\Delta\Phi_B(V)$  is the SBH change due to applied voltage,  $A^*$  is the Richardson constant (32 A/cm<sup>2</sup> K<sup>2</sup> for p-type Si [30]),  $A$  is the junction area,  $k_B T \sim 26$  meV at room temperature,  $\eta$  is the diode ideality factor, defined as the deviation of the measured I-V curve from the ideal exponential behaviour [30], and  $V$  is the external applied voltage. In the low injection regime ( $V < 0.51$  V), the device shows negligible series resistance as highlighted from the linear behaviour shown in Fig. 3(a), however at higher voltages the current deviates from the linearity and  $R_s$  cannot be neglected anymore.  $\Delta\Phi_B(V)$  is significant in reverse bias where a barrier-lowering Schottky due to image force effect occurs [30] but it can be neglected in forward bias where  $\Phi_B \sim \Phi_{B0}$  can be assumed. We estimate SBH in forward bias by fitting the experimental data with Eqs. (3) and (4) and by using  $\Phi_B$ ,  $\eta$  and  $R_s$  as fitting parameters. We get  $\Phi_B = 0.673 \pm 0.003$  eV,  $\eta = 1.16 \pm 0.01$  and  $R_s = 823 \pm 3$  Ω. An ideality factor  $\eta$  close to the unity indicates that the Er/p-Si junction has a behaviour that can be well approximated by the canonical equation of the Schottky junctions.

$\Phi_{B0}$  can also be estimated by the experimental reverse current shown in Figure 3(a) and by reverting Eq. (5) in order to plot  $\Phi_B(V)$ . In the limit  $V \rightarrow 0$  this confirms a value of  $\Phi_{B0} \sim 0.67$  eV. Finally Figure 3(b) shows the SBH dependence on applied reverse voltage and find  $\Delta\Phi_B$  up to  $\sim 0.29$  eV at  $V = -8$  V.

### 3.4. Electro-Optical characterization

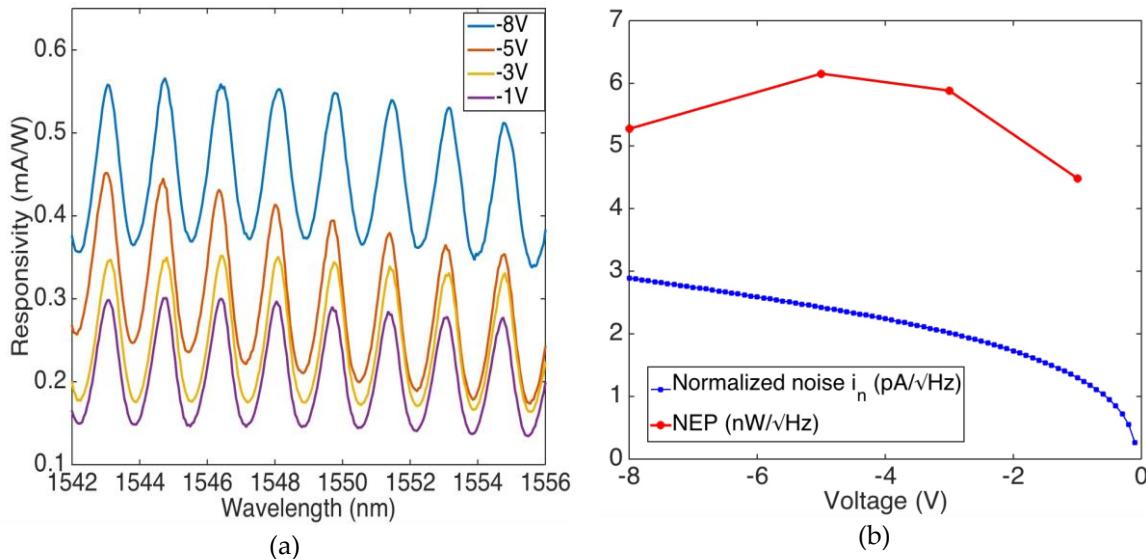
The optoelectronic characterizations are carried out using the setup of Figure 4 (a) and described in Section 2. Figure 4 (b) plots the spectral response under reverse voltage  $V = -1$  V.



**Figure 4.** (a) Optoelectronic measurements setup. (b) Spectral external responsivity Re/Si Schottky PD at  $V = -1$  V.

Device shows many resonance fringes. They are due to the 200μm-thick silicon layer behaves as a low finesse Fabry-Perot microcavity, thus when the wavelength is in agreement with the cavity length the optical field is enhanced in the Si cavity leading to an increased Er absorption. The spectral separation between the peaks is  $\sim 1.7$  nm, matching that one of the Fabry-Perot cavity that is  $FSR = \lambda^2 / 2n_{Si}L = 1.65$  nm, being  $\lambda$  the wavelength, and  $n_{Si}$  and  $L$  the Si refractive index and cavity length, respectively. As expected, at resonance we get photocurrent (responsivity) peaks due to increased absorption at the Er/Si interface. Maximum responsivity is  $\sim 0.3$  at -1V of reverse bias applied.

To further enhance  $R_{ext}$ , we exploit the Schottky barrier lowering effect and apply a larger (up to 8 V) reverse bias to the PDs.



**Figure 5.** (a) Responsivity vs wavelength at different reverse biases; (b) NEP (red circles) and total noise current in (blue squares) at different reverse biases.

Figure 5 (a) plots  $R_{ext}$  for different reverse bias. We get  $R_{ext} \sim 0.55$  mA/W at  $V = -8$  V. It could be useful to mention that these devices show a responsivity more than two order of magnitude higher than same device realized with copper (Cu) [31]. This remark can be partially explained by considering the Er/Si interface is characterized by a reflectivity one order of magnitude lower than copper as shown in Fig. 2(b) and this lead to increased responsivity as shown in Eq. (3).

To estimate a noise figure of our PD we calculate the noise equivalent power (NEP), i.e., the amount of incident light power that generates a photocurrent equal to the noise current,  $NEP = i_n/R_{ext}$  [32]. We assume that Johnson (thermal) and shot (quantum) noise dominating over the low-frequency (1/f) noise [33, 34]. The Johnson ( $i_j$ ) and shot ( $i_s$ ) noise currents normalized to the spectral band [1 Hz] are given by  $i_j = ((4kT)/R_{eq})^{1/2}$  [29] and  $i_s = (2q(I_{ph} + I_d))^{1/2}$  [29], where  $R_{eq} = dV/dI$  is the equivalent resistance of a PD at reverse bias in dark,  $I_{ph}$  is the photocurrent,  $I_d$  is the dark current and  $i_n = i_j + i_s$  is the normalized noise. Figure 5 (b) plots both NEP and  $i_n$  as a function of the reverse bias applied  $V$  and for  $V = -8$  V we get  $i_n \sim 2.9$  pA/Hz<sup>0.5</sup> and  $NEP \sim 5.3$  nW/Hz<sup>0.5</sup>.

#### 4. Conclusion

In conclusion, we have demonstrated the first free-space Er-based PD for operation at 1.55  $\mu$ m. The proposed devices are based on Er/pSi Schottky junctions and their photodetection mechanism is based on internal photoemission. The Er/Si junction has been electrically characterized at room temperatures and a series resistance, ideality factor and Schottky barrier of 823  $\Omega$ , 1.16 and 673 meV have been achieved, respectively. It is worth noting that the ideality factor is close to the unity demonstrating that the Er/pSi junction can be very well described taking advantage of the canonical theory on the Schottky structures.

The PDs are characterized by external responsivity of 0.29 mA/W at 1V; this value increases up to  $\sim 0.55$  mA/W with a reverse voltage of 8V. Finally, normalized noise and NEP, have been discussed.

The results above indicate the possibility of realization of Si-based free-space PDs that operate at 1.55  $\mu$ m taking advantage by a rare earth as Er. To the best of our knowledge, this is the first free-space Er/pSi Schottky PD for operation at 1.55  $\mu$ m. Moreover, it should be noted that the proposed device could be viewed as a low-finesse Fabry-Perot microcavity where the Er absorption, and so device responsivity, can be periodically increased due to the enhancement of the optical field inside the Si

cavity. In this context, the responsivity may be enhanced through use of an high-finesse Fabry-Pérot optical microcavities, which have previously demonstrated capabilities for provision of greatly increased absorption of the active medium [35]. In addition, the use of a high-finesse Fabry-Pérot optical microcavity would also be beneficial in terms of NEP.

We believe that this work paves the way to the fabrication of Er-based both sources and photodetectors to be monolithically integrated on the same Si substrate.

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