

Article

Miniaturized PIFA for 5G Communication Networks

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Abstract: This paper designed a miniaturized Planer Inverted-F Antenna for 5G communication networks including Long Term Evolution Advanced mobile communication services. With showing the radiation pattern, voltage standing wave ratio, and antenna gain of the designed Planer Inverted-F Antenna, this paper evaluates its performance. To show the key characteristics of the Planer Inverted-F Antenna, this paper modeled and simulated it with various variances. Moreover, the real Planer Inverted-F Antenna is fabricated, and measurements were done to validate the simulated characteristics of the internal antenna.

Keywords: antenna; PIFA; LTE; 5G; communication

1. Introduction

Today, the miniaturization of the antenna is becoming increasingly needed due to the small size of the wireless communication system. As the size of the antenna is mainly determined by the wave length, it is difficult to miniaturize the antenna for current mobile communication services. To overcome this difficulty, the method of using dielectric materials with high permittivity to miniaturize the antenna has been studied by many researchers [1-11]. However, this method causes a decline of the antenna gain due to the decline of the radiation effectiveness and dielectric loss. With this reason, the needs for studying the miniaturization of the antenna by modifying the structure of the antenna, not by using dielectric materials, have been increased. Therefore, this paper suggests a new method for designing a compact multi-band internal antenna with a patch and a ground plane for common mobile communication services. A patch antenna is one of low profile radio antenna, which can be installed on a flat surface. It consists of flat metal patch that mounted over a ground plane. Patch antennas has simple structure to fabricate, to modify and to customize. The original type of the patch antenna is a microstrip antenna. Two metal plates form a resonance in microstrip transmission lines which has a length of approximately one-half wavelength of the radio waves, and, at these microstrip transmission line, the radiation occurs due to discontinuities. The radiation at the microstrip transmission lines gives the antenna larger electric field area than its physical dimensions, which means the antenna can be resonant. Usually, the length of microstrip transmission line is slightly shorter than one-half a wavelength at the interested frequency, and a patch antenna is built on a dielectric plate. The designed multi-band internal antenna can cover the frequency bands for Global System for Mobile communications (GSM), Digital Cellular System (DCS), Personal Communications Service (PCS), Wideband Code Division Multiple Access (WCDMA), Long Term Evolution (LTE) communication services, and 5G communication networks. As mentioned above, there are many methods for the miniaturization of the antenna. In consideration of the antenna gain and the effectiveness, modifying the structure of the antenna is better method to miniaturize the size of the antenna than using dielectric materials with high permittivity. With this reason, this paper suggests a new structure of a compact multi-band internal antenna for mobile handsets for WCDMA800, WCDMA850, GSM900, DCS, PCS, WCDMA2100, LTE2100 communication services, and 5G communication networks.

This paper is organized as follows. In Section 2, we design a multi-band internal antenna for various mobile communication services. In Section 3, we introduce a coordinate system for analyzing various antenna characteristics. Afterwards, we simulate and measure antenna

characteristics, including antenna gain, voltage standing wave ratio (VSWR), and radiation pattern, in Section 4 and 5. Finally, we conclude the paper and lay out our future research plan on related topics in Section 6.

2. Long Term Evolution Advanced Mobile Service

A Planer Inverted-F Antenna (PIFA) is about half size of general dipole antenna and has a conductor layer in it as a ground layer. The relationship between broad band width characteristics and the thickness of the material can be determined by the following equation.

$$BW = \frac{Ah}{\lambda_0 \sqrt{\epsilon_r}} = \sqrt{\frac{W}{L}} \quad (1)$$

for $A=180$:

$$\frac{h}{\lambda_0 \sqrt{\epsilon_r}} \leq 0.045$$

for $A=200$:

$$0.045 \leq \frac{h}{\lambda_0 \sqrt{\epsilon_r}} \leq 0.075$$

for $A=220$:

$$0.075 \leq \frac{h}{\lambda_0 \sqrt{\epsilon_r}}$$

and

$$D \cong 0.2W + 6.6 + 10 \log\left(\frac{1.6}{\sqrt{\epsilon_r}}\right) dB. \quad (2)$$

Where BW is a broad band width, A is the area of the dielectric material, h is the thickness of the dielectric material, λ_0 is the wavelength, ϵ_r is the dielectric permittivity, D is the directivity of the antenna, W and L are the width and length of the radiating element in a PIFA respectively [12]. As Eq.1 shows, the frequency band for a broad band width is proportional to the thickness of the material and is inversely proportional to the dielectric permittivity. And also, Eq. 2 shows that the directivity of the antenna decreases as the dielectric permittivity increases. In designing the multi-band internal antenna, as the thickness of the dielectric material increases, the broad band characteristic of the antenna is improved. However, this also makes the width of the microstrip line increase, which means the unwanted radiation occurs from the feed. To solve this problem, this paper suggests the structure of the multi-band internal antenna as shown in Figure 1, and the designed multi-band internal antenna is shown in Figure 2.

3. Planer Inverted-F Antenna

In this paper, the multi-band internal antenna for WCDMA800, WCDMA850, GSM900, DCS, PCS, WCDMA2100, LTE2100 mobile communication services, and 5G communication networks is modeled, and the antenna characteristics are simulated with the coordinate system.

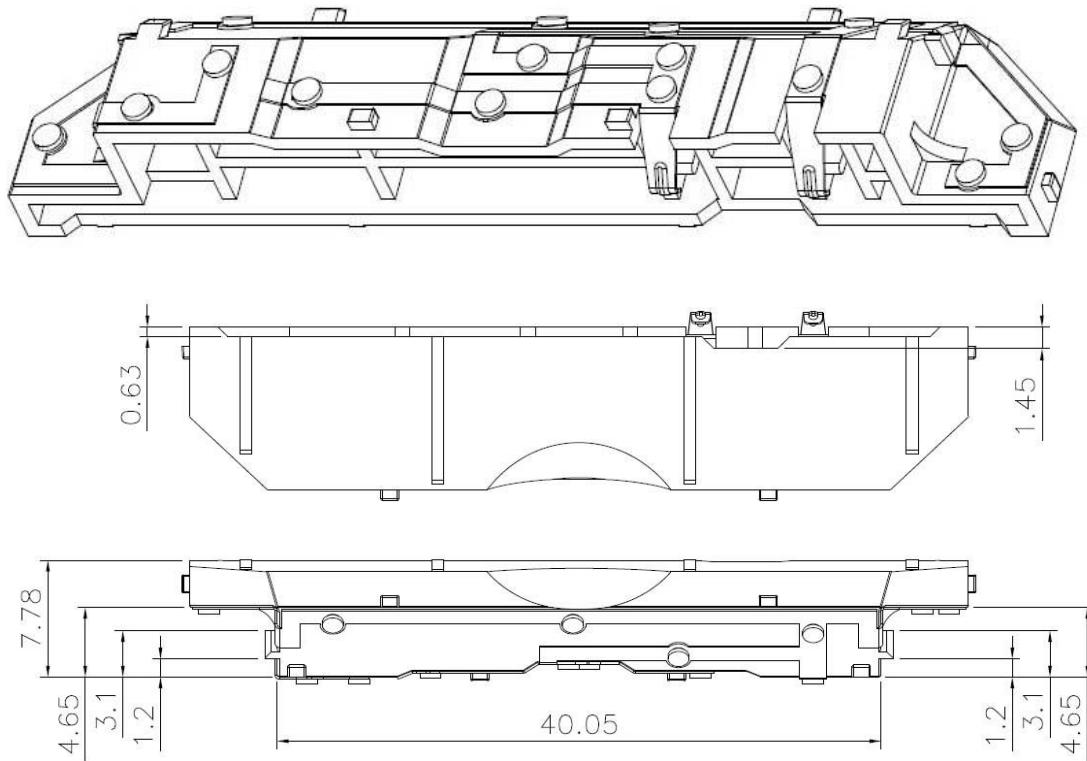


Figure 1. Structure of the PIFA.



Figure 2. Fabricated PIFA.

4. Simulation

For the simulations, High Frequency Structure Simulator (HFSS) program ver. 11 is used to analyze the designed multi-band internal antenna for mobile communication. The radiation pattern of the multi-band internal antenna is simulated at H-plane, E1-plane, and E2-plane respectively, and the simulated radiation patterns are as shown in Figure 3-5.

As mentioned above, this paper suggests the multi-band internal antenna for WCDMA800, WCDMA850, GSM900, DCS, PCS, WCDMA2100, LTE2100 mobile communication services, and 5G communication networks. Figure 4-6 show the radiation pattern of the internal antenna at 824 MHz - 2.17 GHz frequency band. To prove the antenna characteristics of the designed multi-band internal antenna in numerical value, Table 1 and 2 show the voltage standing wave ratio (VSWR) and the peak gain of the antenna at each frequency band, and the radiation pattern of the antenna is almost omni-directional as shown in Figure 3-5. In the simulation of the radiation pattern, the impedance bandwidth is set from 824 MHz to 2.17 GHz, and the insertion loss is the minimum at 960 MHz. Although the simulated radiation patterns at H-plane and E-plane are not symmetric patterns, they show forward and backward patterns. Moreover, the radiation patterns are the maximum at the perpendicular direction to the antenna side.

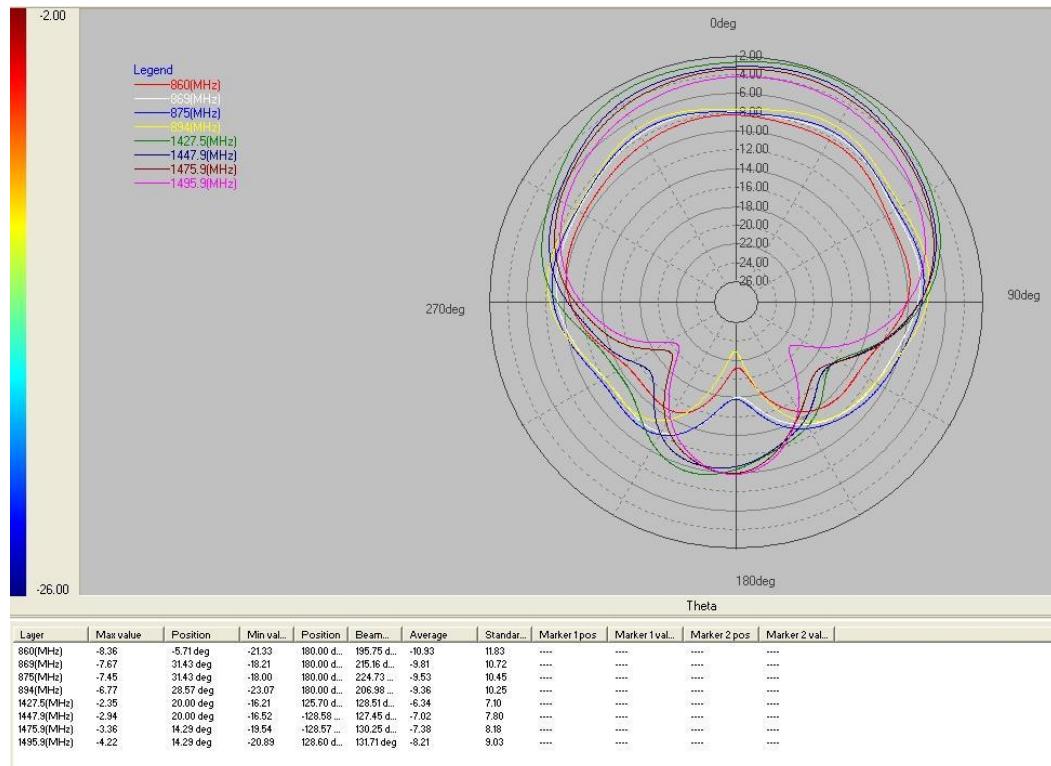


Figure 3. Radiation Pattern (H-Plane).

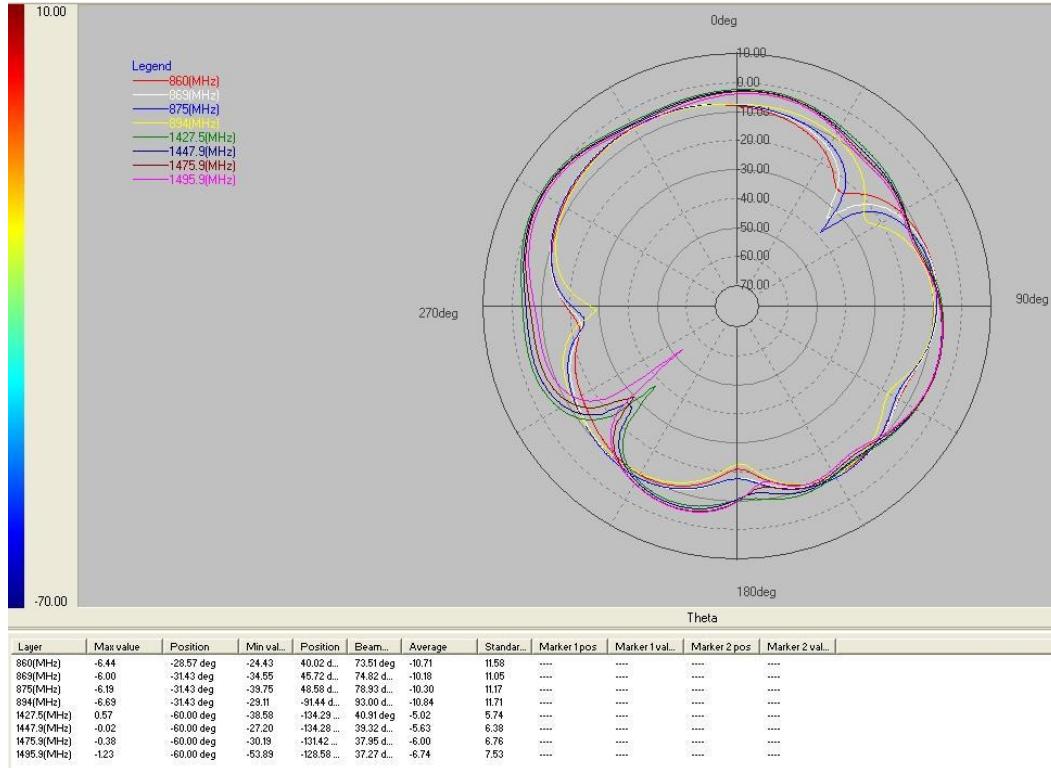


Figure 4. Radiation Pattern (E1-Plane).

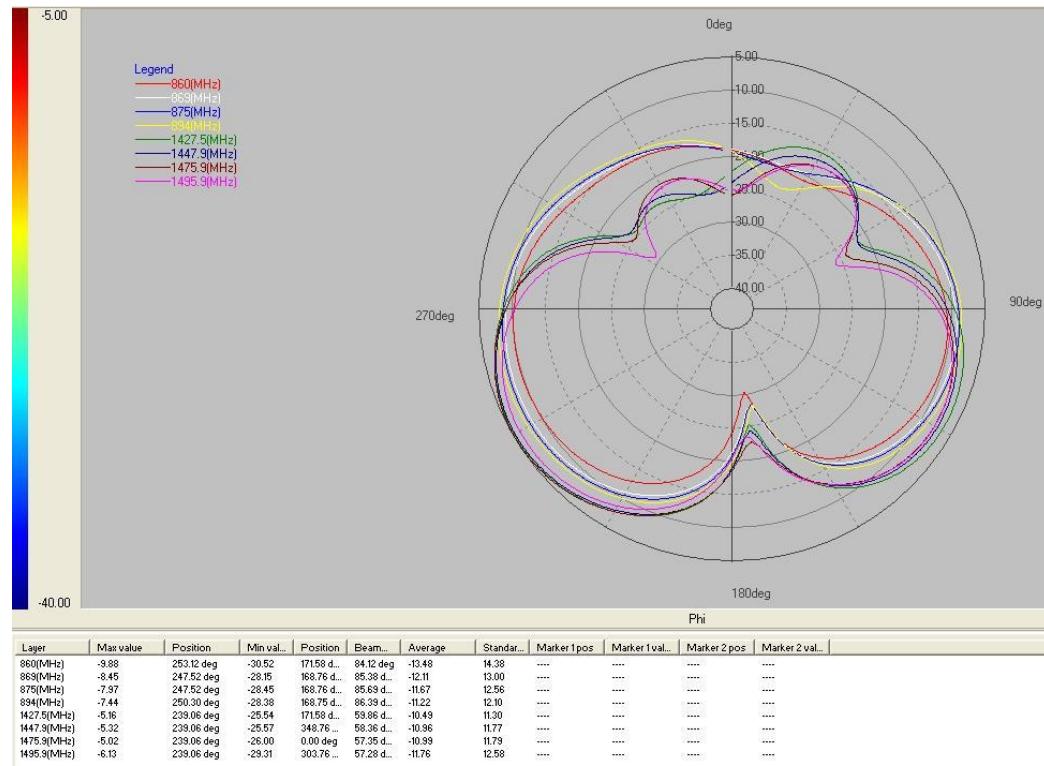


Figure 5. Radiation Pattern (E2-Plane).

Table 1. Simulation Result (VSWR).

Frequency range	W800, W850, GSM900		DCS, PCS, WCDMA2100, LTE2100		
	824 MHz	960 MHz	1710 MHz	1920 MHz	2170 MHz
VSWR [dBi]	6.3	7.2	5.8	2.7	2.9

Table 2. Simulation Result (Peak Gain).

Frequency range	W800, W850, GSM900		DCS, PCS, WCDMA2100, LTE2100			
	824 MHz	960 MHz	1710 MHz	1920 MHz	2170 MHz	
Peak gain [dBi]	H-plane	0.4	-4.3	-3.1	0.0	-1.0
	E1-plane	0.8	-5.6	-2.2	1.4	2.6
	E2-plane	1.4	-4.4	-2.7	1.5	3.0

5. Measurement

The simulated multi-band internal antenna is fabricated, and the VSWR and gain of the internal antenna were measured as shown in Figure 6. For the measurement system, a network analyzer (Agilent 5071B), a calibration kit (Agilent 85033E), an adaptor (SMA Female ↔ SMA Male), and a

measurement cable (SMS-SF141) are used. The method and procedure of the measurement are as follows. The shielded box is set to the port of the network analyzer, and the calibration for them is done. After setting the fabricated antenna to the set JIG and unit JIG, the set JIG is connected vertically to the port inside the shielded box and the unit JIG is connected horizontally to the port inside the shielded box respectively. With the calibration of the network analyzer, the coaxial cable from the set JIG and unit JIG are connected to the port inside the shielded box. In the whole measurement procedure, the measurement should be performed on the non-conductive table. As shown in Figure 7 and 8, the measured VSWR satisfies the common use specification for the WCDMA800, WCDMA850, GSM900, DCS, PCS, WCDMA2100, LTE2100 mobile communication services, and 5G communication networks[13-15].

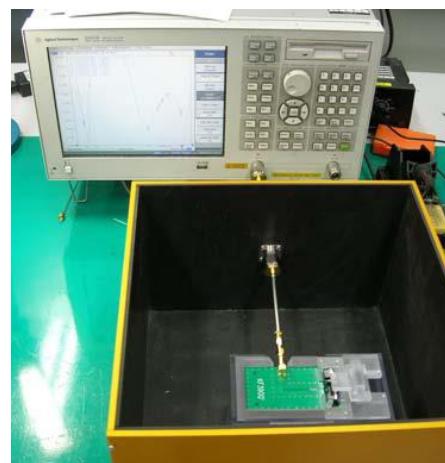


Figure 6. Measurement Setup.

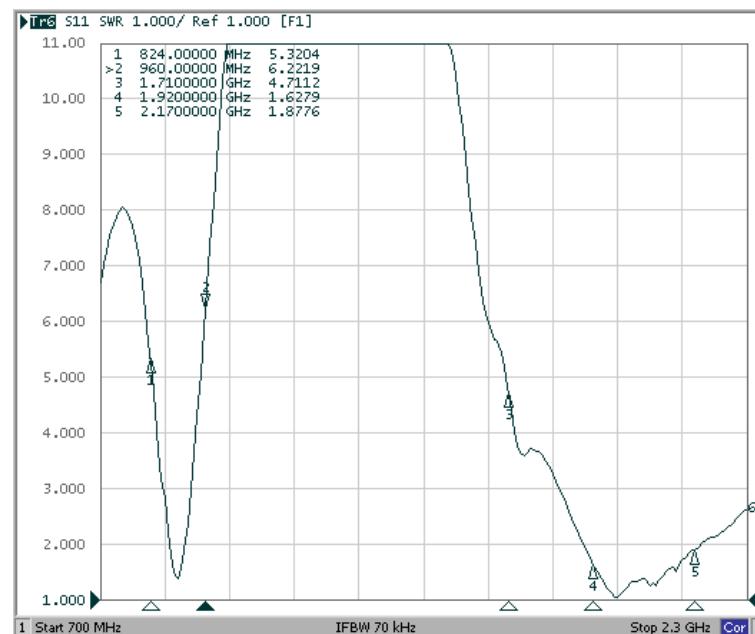


Figure 7. Measurement Result (VSWR).

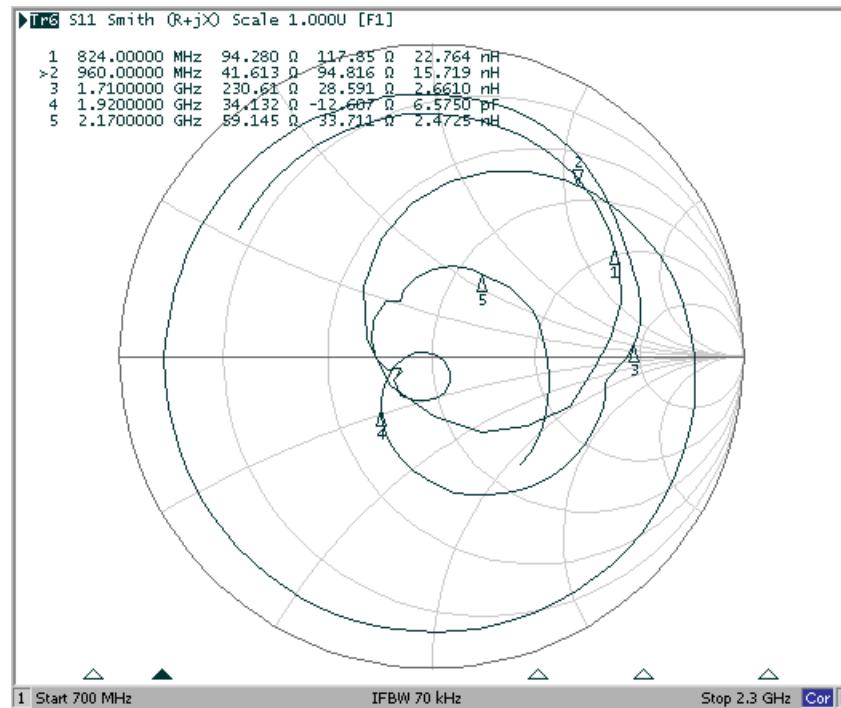


Figure 8. Measurement result (Smith Chart).

6. Conclusion

A compact multi-band internal antenna for mobile handsets which can cover WCDMA800, WCDMA850, GSM900, DCS, PCS, WCDMA2100, LTE2100 communication services, 5G communication networks is modeled, simulated, and measured in this paper. This multi-band internal antenna shows a satisfactory performance for a common application. The beam width at E-plane radiation pattern is about 120°, and the gain is 5.6 dBi at 960 MHz. The radiation patterns at E-plane from 824 MHz to 2.17 GHz have similar patterns, and a side lobe is formed at H-plane as the frequency increases. However, this side lobe is considered not to be a big problem because it is comparatively very small to the main beam which is vertical to the antenna side. Therefore, the designed multi-band internal antenna in this paper can satisfy the broadband characteristics in the view of an impedance, radiation pattern, and gain.

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Abbreviations

The following abbreviations are used in this manuscript:

WCDMA Wideband Code Division Multiple Access

GSM Global System for Mobile Communications

DCS Digital Cross-connect System

PCS Personal Communication Services

SMA Sub Miniature version A

References

1. Yan, Y.; Jiang, X.; Lee, M.H. A grouped decoding algorithm for non-binary LDPC code with quasiorthogonal STBC in MIMO System. *JCIT.* **2013**, *8*, 763-772.
2. Chen, J.; Li, J.; Zhu, Y.; Joint location and velocity estimation for high speed target in multi-carrier-frequency MIMO radar. *AISS.* **2013**, *5*, 223-229.
3. Lin, C.H.; Lai, L.G.; Tiong, K.K.; Sun, J.S.; Chen, G.Y. A novel on-glass GPS antenna for handset applications. *IJACT.* **2013**, *5*, 165-171.
4. Zeng, W.; Zhao, J. Microstrip yagi-uda antenna for 2.45 GHz RFID handheld reader. *JDCTA.* **2012**, *6*, 285-292.
5. Wu, Y.; Peng, X.; Hu, Z. Efficient solution for interference alignment in the 3-user MIMO interference channel. *AISS.* **2012**, *4*, 176-183.
6. Gao, Y.; Chen, X.; Ying, Z.; Parini, C. Design and performance investigation of a dual-element PIFA array at 2.5 GHz for MIMO terminal. *IEEE Trans. Antennas Propag.* **2007**, *55*, 3433-3441.
7. Foschini, G. Layered space time architecture for wireless communication in a fading environment when using multi element antennas. *Bell Labs Technical Journal*, **1996**, *1*, 41-59.
8. Wallace, J.; Jensen, M.; Swindlehurst, A.; Jeffs, B. Experimental characterization of the MIMO wireless channel: data acquisition and analysis. *IEEE Trans. Wireless Commun.* **2003**, *2*, 335-343.
9. Stutzman, W.L.; Thiele, G.A. *Antenna theory and design*, 3rd ed.; John Wiley & Sons: USA, 2012; pp.564-570.
10. Thaysena, J.; Jakobsen, K. Mutual coupling between identical planar inverted-F antenna. *AEU-INT J ELECTRON C*, **2007**, *61*, 540-545.
11. Chattha, H.T.; Huang, Y.; Lu, Y. PIFA bandwidth enhancement by changing the widths of feed and shorting plates. *IEEE Antennas Wireless Propag. Lett.* **2009**, *8*, 637-640.
12. Hirasawa, K.; Haneishi, M. *Analysis, design, and measurement of small and low-profile antennas*, Artech House Antenna Library: UK, 1991; pp.170-175.
13. Chang, C.H.; Wong, K.L. Printed $\lambda/8$ -PIFA for penta band WWAN operation in the mobile phone. *IEEE Trans. Antennas Propag.* **2009**, *57*, 1373-1381.
14. Chiu, C.Y.; Shum, K.M.; Chan, C.H. A tunable via-patch loaded PIFA with size reduction. *IEEE Trans. Antennas Propag.* **2007**, *55*, 65-71.
15. Rhee, E.; Lee, J. Enhanced multi-band internal antenna for mobile communication. *JDCTA.* **2013**, *7*, 158-164.