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Article

# Novel Field-Free Line Generator for Mechanically Scanned Magnetic Particle Imaging

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**Abstract:** In this study, we propose an efficient field-free line (FFL) generator for mechanically driven FFL-magnetic particle imaging (MPI) applications. The novel FFL generator comprises pairs of Halbach arrays and bar magnets. The proposed design generates high-gradient FFLs with low-mass permanent magnets, realizing fine spatial resolutions in MPI. We investigate the generated magnetic field using simulations and experiments. Our results show that the FFL generator yields a high gradient of 4.76 T/m at a cylindrical field of view of 30 mm diameter and a 70 mm open bore. A spatial resolution of less than 3.5 mm was obtained in the mechanically driven FFL-MPI.

**Keywords:** field-free line; magnetic particle imaging; frequency mixing magnetic detection

## 1. Introduction

Magnetic particle imaging (MPI) is a tracer imaging technique that detects the positions and densities of injected magnetic particles via the nonlinear magnetic response [1]. Iron-oxide tracers are safe for humans and circulate through the blood stream without producing any ionizing radiation. Thus, MPI has attracted significant research attention with regard to medical applications [2,3].

Existing MPI techniques usually require fine spatial resolution, which largely depends on the gradient strength of the selection field. Particularly, the selection field is an inhomogeneous magnetic field with an unsaturated magnetic field area, wherein the magnetization change caused by a drive field is generated selectively. A field-free point (FFP) or a field-free-line (FFL) are usually employed for selection fields. As the gradient of the selection field increases, the size of the region in which the tracers respond to the excitation field decreases [4]. This results in a narrower spatial resolution of MPI. Additionally, FFL-MPI exhibits better sensitivity than commonly used FFP-MPI by approximately one order of magnitude [5].

FFL systems have been realized using current-driven coils, permanent magnets, or combinations of the two [2–6]. Coil-based FFL generators are advantageous in that it is easy to construct open bores, and fast scanning can be realized with rapid control of the magnetic field strength by a current. However, coil-based FFL generators consume a large amount of power when shifting the high gradient selection field, even for small bore sizes [7]. Recently, Halbach arrays have been utilized in FFL generators for MPI. Halbach arrays use permanent magnets instead of electromagnets, which reduces the power consumption [8–10]. However, the FFL is moved electronically by current-driven coil configurations, involving high power consumption when the field of view (FOV) is larger. The high power consumption is a critical issue to be resolved in realizing FOVs suitable for imaging large sections of the human body. Additionally, the large amplitude and high frequency required for the drive field invoke severe health concerns and generate significant noise [11].

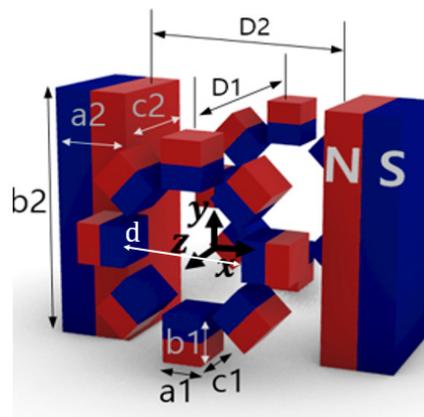
The scanning speed of mechanically driven MPI is lower than that of electronically controlled MPI. Nevertheless, recent high-tech motor stages are sufficiently fast and robust, such that 2D MPI scanning can be performed in a few seconds. Despite the time consumed to achieve a high temporal

resolution, MPI is still useful in diverse applications. For example, recent studies have investigated MPI as a continuous clinical monitoring tool for substituting conventional CT and MRI [12,13]. Notably, CT cannot be employed for recurrent monitoring owing to radiation exposure, and MRI entails a substantially long examination time. Consequently, the imaging time of MPI, which is only a few minutes, will not be a critical limitation in fields that require long-term, repeated monitoring.

Here, we propose a novel FFL generator for mechanically driven FFL-MPI based on pairs of Halbach arrays and bar magnets. To the best of our knowledge, our permanent magnet-based FFL configuration is the first of its kind. The FFL generator exhibits a high gradient with a large open bore. The magnetic field characteristics of the proposed FFL generator and the principle of the FFL formation will be examined with simulation results. In addition, the linear and rotational movement characteristics of the FFL for mechanical FFL-MPI will be explained. Finally, the MPI application results obtained in the mechanically driven manner based on this FFL generator are shown.

## 2. Materials and Methods

The proposed FFL generator is shown in Figure 1. It comprises pairs of Halbach ring-type arrays and bar-shaped magnets. For ease of construction, we set the bore size to 70 mm. The dimensions of the FFL device with a 70 mm open bore are detailed in Table 1, and we used an NdFeB (N35 grade) magnet. In this configuration, the field gradient is 4.76 T/m along the x and z axes. The detailed geometric values of this FFL generator are presented in Table 1.



**Figure 1.** Configuration of the proposed FFL generator (d: inner diameter of Halbach ring, D1: distance between Halbach ring pair, D2: distance between bar-shaped magnet pair, [a1, b1, c1]: dimensions of small magnets of Halbach ring, [a2, b2, c2]: dimensions of bar-shaped magnets).

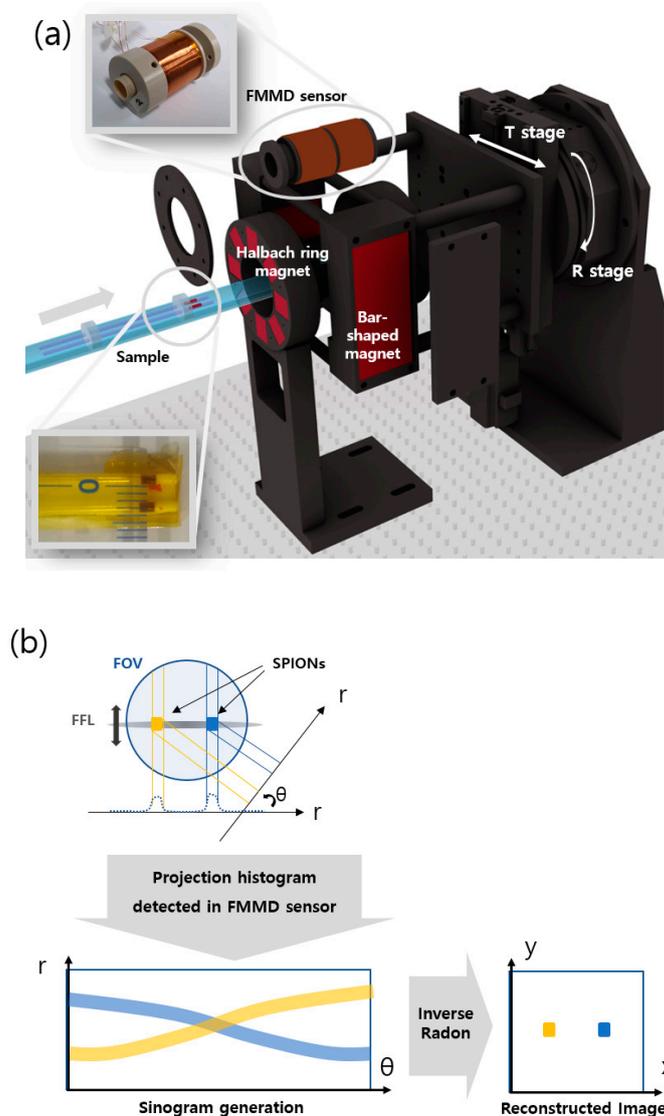
**Table 1.** Dimension of the FFL device with 70 mm open bore (d: inner diameter of Halbach ring, D1: distance between Halbach ring pair, D2: distance between bar-shaped magnet pair, n1: number of small magnet of Halbach ring, [a1, b1, c1]: dimensions of small magnets of Halbach ring, [a2, b2, c2]: dimensions of bar-shaped magnets)

Aperture size [mm]	Geometry (d, D1, D2, n1, [a1, b1, c1], [a2, b2, c2]) [mm]	Magnetic field gradient (Simulation /Measured)	Magnet weight (Total/ Bar magnets)	FOV
70	(74, 112, 70, 8, [30, 25, 30] [160, 70, 50])	4.76 T/m / 4.6 T/m	9.55 kg / 7.59 kg	30×30×100 mm <sup>3</sup>

To analyze the magnetic field of the proposed FFL generator and its movement, we performed simulations with the three-dimensional (3D) Faraday software (Faraday V10.2 Enginia Research Inc, MB, Canada) using a computer with an Intel i7-8700K CPU and Windows 10 operating system. The FFL generator was constructed based on the simulation results, and the generated magnetic field was

measured using a 3-axis Hall-effect sensor (name, company) connected to a robotic device translating a regular distance in three dimensions.

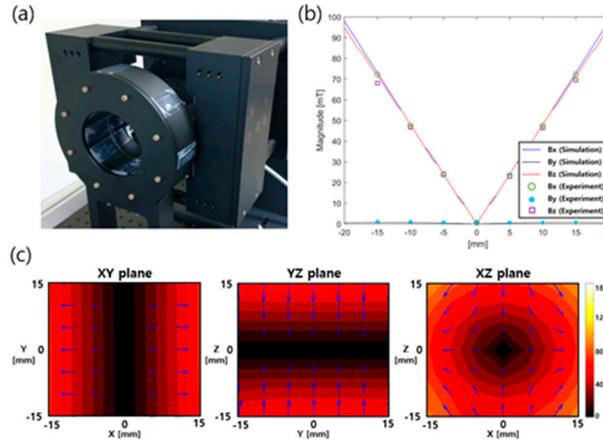
Mechanically driven FFL-MPI was realized with rotational and translational stages (Namil Optical Instruments Co. Incheon, Korea). The excitation and detection superparamagnetic iron-oxide nanoparticles (SPIONs) signals were evaluated based on the frequency mixing magnetic detection (FMMD) technique [6]. The experimental setup for MPI is shown in Figure 2. The Halbach array pair is mounted on the optical table, and the bar magnet pair is mounted on the rotational and translational (R&T) stages. The linear stage moves the sample into the FFL position inside the FMMD sensor. Signal generation and detection are carried out using an FMMD sensor reported previously [14]. The measured signal generates a sinogram, while the FFL scans the sample translationally and rotationally. Then, the sinogram data can be reconstructed into 2D images via the inverse Radon transform. The SPIONs used for the MPI sample were Synomag-D (product no. 104-00-501) from Micromod (Rostock, Germany). A thin capillary tube was filled with the SPIONs. The outer and inner diameters of the tube are 1.5 mm and 1.2 mm, respectively.



**Figure 2.** MPI system with the proposed FFL generator. (a) 3D rendering of the setup, (b) schematic illustration of the measurement mode of rotating the FFL by an angle  $\theta$ , yielding a sinogram from which the image is reconstructed.

### 3. Results and Discussion

Figure 3 (a) shows a photograph of the constructed FFL device. The magnets are positioned in an aluminum casing, in accordance with the simulation dimensions listed in Table 1. The FFL generator and all casing components such as bolts are constructed from nonmagnetic materials such as aluminum, so that the generated FFL magnetic field is not interfered with. The magnetic field was measured using a Hall-effect sensor positioned on a 3D moveable robotic arm. Figure 3 (b) shows a comparison of the measured magnetic field along the x, y and z axes with the simulation results. The scanning area was  $[-15 \text{ mm}, 15 \text{ mm}]$  along each axis at 5 mm intervals. The measured contour map is shown in Figure 3 (c). The measured data are well matched with the simulation results.



**Figure 3.** Experimental results of the FFL generator: (a) Photograph of the crafted FFL generator with aluminum casing, (b) Measured gradient strength compared with simulation results, (c) Measured 2D contour graph of the magnetic field of the FFL generator.

The generation of clear FFL of our new device as shown in Figure 3 can be explained with the superposition principle of magnetic fields. The FFL generator are composed of the Halbach ring pair and the bar-shaped magnet pair, and the superposition of the magnetic fields of all the components explains the creation of FFL.

The magnetic field simulation results for the Halbach ring pair and the bar-shaped magnet pair are shown in Figure 4(d) and (f), respectively in the x-y, y-z, and x-z planes near the center. The FFL field generated from the bar magnet and Halbach ring pairs can be approximated as

$$H_{FFP}^x = \begin{pmatrix} G_{xh} & 0 & 0 \\ 0 & G_{yh} & 0 \\ 0 & 0 & G_{zh} \end{pmatrix} r_0, \quad H_{FFP}^z = \begin{pmatrix} G_{xb} & 0 & 0 \\ 0 & G_{yb} & 0 \\ 0 & 0 & G_{zb} \end{pmatrix} r_0, \quad (1)$$

where  $r_0 = [x, y, z]^T$  is the spatial position vector, G represents the gradient matrix, the subscripts x, y, and z denote the directions, and h and b denote the Halbach ring pair and the bar magnet pair, respectively.

The net magnetic field resulting from the superposition of the magnetic fields generated from the two components is expressed as

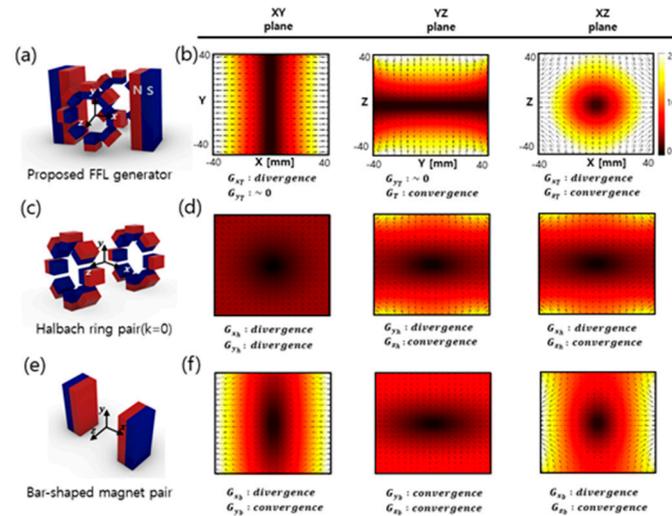
$$H_{FFL}^y(r) = H_{FFP}^x(r) + H_{FFP}^z(r) = \begin{pmatrix} G_{xh} + G_{xb} & 0 & 0 \\ 0 & G_{yh} + G_{yb} & 0 \\ 0 & 0 & G_{zh} + G_{zb} \end{pmatrix} r_0 = \begin{pmatrix} G_{xh} + G_{xb} & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & G_{zh} + G_{zb} \end{pmatrix} r_0, \quad (2)$$

where  $G_{yh} \sim -G_{yb}$ .

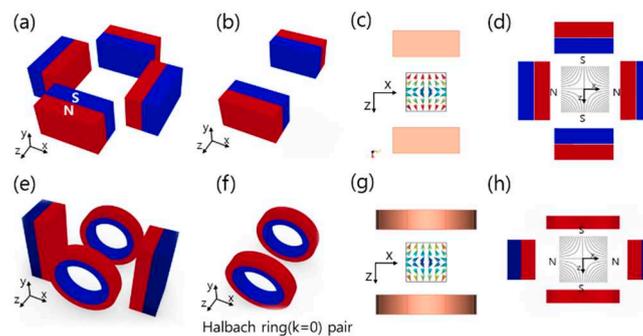
When the  $G_{yh}$  has a similar magnetic field value as  $G_{yb}$  and opposite vector direction, the superposition of them generates zero field, as illustrated in Eq. (2).

The newly proposed FFL generator is based on quadrupole magnets. Figure 5 (a) shows that when the quadrupole magnets are stacked symmetrically to the y axis, the FFL is generated along the y axis. Figure 5 (e) is a transformed design of Figure 5 (a) where the square magnet pair of Figure 5

(a) is substituted with a pair of Halbach rings. The magnetic field generated by the Halbach ring pair is similar to that of the square magnet pair, as shown in Figure 5 (b) and (f); therefore, a FFL is also generated by the magnet structure of Figure 5 (e).



**Figure 4.** Proposed FFL generator and FFL characteristics. (a) Schematics of the FFL generator, (b) FFL 3D contour graph of the FFL generator, (c) magnet arrangement of a pair of Halbach rings, and (d) FFL 3D contour graph of its field, (e) bar magnet pair, and (f) FFL 3D contour graph of its field.



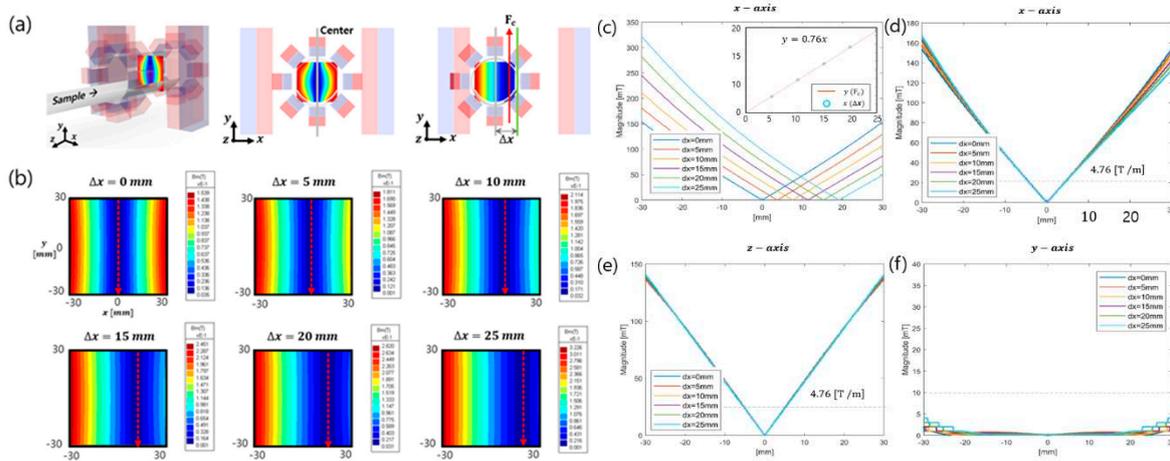
**Figure 5.** Comparison of quadrupole magnets and proposed FFL generator: (a) quadrupole magnets, (b) Square magnet pair, (c) magnetic field of square magnet pair, (d) magnetic field of quadrupole magnet, (e) proposed FFL generator, (f) Halbach ring pair (g) magnetic field of the pair of Halbach rings, (h) magnetic field from proposed FFL generator.

We modified the cylindrical Halbach ring to a combination of small square magnets. This is done because both show similar magnetic characteristic in simulation study, but the fabrication with the square magnets provides more benefits in experiment. First, the cylinder-shaped magnets need to be custom-manufactured, whereas the square magnets are readily available on the market in a variety of sizes. Also, the radius is fixed when using cylinder-type magnets, but the combination of square magnets can easily be adjusted to the radius of the aperture by changing their number and their spacing. In addition, square magnets allow easier adjustment of magnet strength by overlapping several of them. Thus, square magnets were selected for Halbach ring pair fabrication instead of cylinder-type magnets. As a result, a clear straight FFL was found both in simulation and experiment, as shown in Figure 4 and Figure 5.

As next step, we tried to check whether a MPI system that does not require a drive coil can be implemented using the above newly designed FFL generator. The important thing here is that the inner diameter of Halbach ring pair is designed to the same value as the outer diameter of the FMMD sensor for MPI, so that the Halbach ring pair cannot move along the x and y axes for the movement of the FFL. Therefore, it is necessary to check whether the movement of the FFL is possible only by

the movement of the bar magnet. In the simulation study with Faraday SW, the FFL movement and gradient strength were confirmed when just moving the bar magnet pair.

Figure 6 (a) shows a schematic of the translational movement of the FFL. A simulation was conducted such that the bar magnet pair moves in the positive  $x$  direction up to 25 mm in increments of 5 mm. Figure 5 (b) shows the two-dimensional simulation results of the magnetic field along the  $x$ - $y$  plane. It can be seen that the FFL shifts to the traveling direction of the bar magnet while translating.



**Figure 6.** Linear movement of the FFL and gradient strength: (a) translation movement of the bar magnet pair, (b) contour map along the  $x$ - $y$  plane, magnetic strength along the (c, d)  $x$ -axis, (e)  $z$ -axis, (f)  $y$ -axis while the bar magnet pair is displaced ( $\Delta x$ ) from 0 mm to 25 mm.

To determine whether the FFL field gradient is sustained when the bar magnet pair is displaced, the field gradient along the  $x$ ,  $y$ , and  $z$  axes is investigated at each shift from 5 mm to 25 mm. Figure 6 (c), (e), and (f) show the field magnitudes along the  $x$ ,  $y$ , and  $z$  axes. Figure 6 (d) illustrates the overlapping data shown in Figure 6 (c), which was obtained to compare the field gradient along the  $x$  axis. As shown in Figure 6 (d), (e), and (f), the gradient of the FFL was maintained with the same value when the bar magnet pair moved. Even though the  $y$  axis gradient shows a remnant field as the pair moves outside the center position, the value is much smaller than the saturation field strength of approximately 10 mT. Thus, the field gradient is negligible.

The displacement of the FFL center ( $F_c$ ) is linearly proportional to the bar magnet displacement ( $\Delta x$ ), as shown in Figure 6 (c). The relation can be described by  $y = ax$ . This is because the gradient is the sum of the magnetic field due to the Halbach array pair and the bar magnet pair. The magnetic field of the bar magnet pair along the  $x$  axis near the zero position is approximately given by  $y_b = G_{x_b}(x - \Delta x)$ , and  $y_h = G_{x_h}x$  for the Halbach array pair.

The sum of these components, which is the total magnetic field along the  $x$  axis, is given by

$$y_t = G_{x_b}(x - \Delta x) + G_{x_h}x = (G_{x_b} + G_{x_h})x - G_{x_b}\Delta x, \quad (3)$$

The relation between  $F_c$  and  $\Delta x$  is obtained by setting  $y_t$  to zero and substituting  $x$  with  $F_c$ . The relation is given by

$$F_c = G_{x_b}/(G_{x_b} + G_{x_h})\Delta x, \quad (4)$$

This explains the proportionality between  $x$  and  $F_c$ , and the slope is determined by  $G_{x_b}$  and  $G_{x_h}$ . The gradients used in the simulation are  $G_{x_b} \sim 4$  and  $G_{x_h} \sim 1.25$ , yielding  $a = 0.76$ . This result implies that the MPI raw data can be acquired with the same spatial resolution as that during the linear movement of the FFL.

The rotational movement of the FFL can be realized by rotating the bar magnet pair about the  $z$  axis. As shown in Figure 3 (b), the magnetic field of the Halbach ring pair along the  $x$ - $y$  plane represents the isotropic features. This means that when the Halbach ring pair rotates along the  $z$  axis by any angle, the  $x$ - $y$  plane field map shows the same results at any angle. Therefore, the rotation of

the bar magnet can be considered as the rotation of the entire structure. As a result, the rotation angle of the bar magnet is the same as the rotation angle of the FFL.

The simulation results show that a sharp FFL can be generated by Halbach arrays and bar magnets, and the FFL can be linearly and rotationally moved simply by moving the bar magnet pair. These characteristics make the proposed FFL generator suitable for mechanically driven-MPI applications. Above all, as the Halbach array can remain fixed during the MPI scanning, a compact and high-resolution MPI system can be developed. If the Halbach array has to move with both linear and rotational motions for MPI scanning, its aperture size should include additional space for linear motion without overlapping samples. In contrast, the FFL can be moved only by the movement of the bar magnet while the Halbach array is fixed; therefore, the aperture size of the Halbach array needs to be greater than the maximum diameter of the sample. When designing an FFL-generating device using a permanent magnet, it is advantageous to create a strong FFL gradient when the magnet is close to the FFL position. Consequently, it is beneficial to develop an FFL device with a stronger magnetic gradient and a high-resolution MPI system by using the combination of fewer magnets with a fixed Halbach array and a moving bar magnet.

Finally, we experimentally verified whether MPI images can be successfully obtained with the combination of the fixed Halbach array and the moving bar magnet, as shown by the above simulations. The spatial resolution of the MPI image was also checked. The configuration of the experimental setup is shown in Figure 2. The Halbach array was fixed to the optical table, and the pair of bar magnets were fixed to the R&T stage and moved linearly and rotationally with the stage.

The SPIONs were filled in a very thin capillary tube, with the outer and inner diameters of 1.5 and 1.2 mm, respectively. To measure the resolution, MPI experiments were performed when the intervals of the capillary filled tube samples were 2 mm and 1 mm. As shown in Figure 7, when the distance between the samples was 2 mm, the two spaces were clearly separated in the sinogram. The sinogram was converted into a 2D image through inverse Radon transformation, and it was confirmed that the response of the SPIONs was clearly separated into two spots. When the distance between the samples was 1 mm, the response signals were only faintly separated in the sinogram; however, the boundary of the SPIONs was not clearly visible in the 2D transformed image, as shown in Figure 7(b).

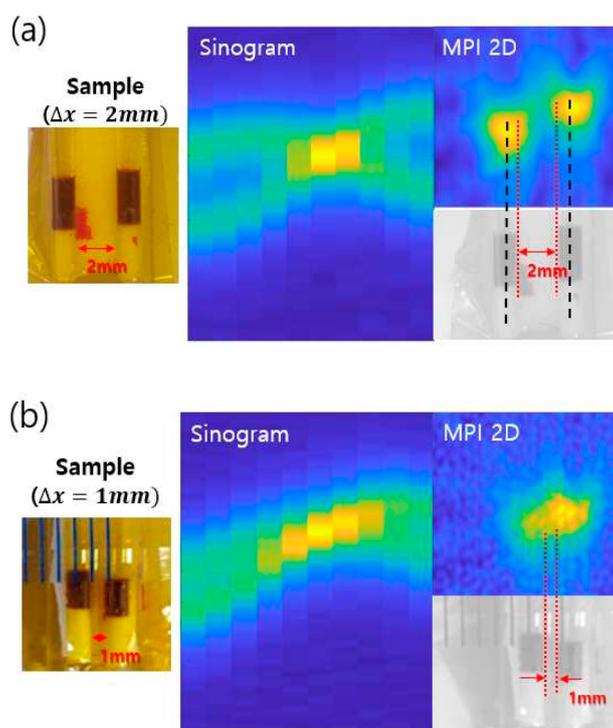


Figure 7. MPI results with sample distance ( $\Delta x$ ) (a) 2 mm and (b) 1 mm.

Thus, it has been shown for the first time that MPI images can be successfully obtained by combining a fixed Halbach array and a moving bar magnet. In this experiment, a new type of FFL generator was fabricated with less than 10 kg of magnets, which can accommodate samples up to a height of 70 mm. The 2D MPI has a spatial resolution of 3.5 mm upon mechanically moving the FFL.

#### 4. Conclusions

We introduced a novel FFL generator comprising pairs of Halbach arrays and bar magnets. The manufactured FFL generator shows a high gradient of 4.76 T/m at a 30 mm diameter cylindrical FOV with a 70 mm open bore and a total magnet weight of under 10 kg. In the MPI implementation of this FFL generator, the obtained 2D MPI image showed a spatial resolution of less than 3.5 mm. This result shows that the combination of Halbach array and bar magnet pairs in the FFL generator is beneficial for realizing a compact and high-performance MPI system.

Mechanically driven MPI with the proposed FFL generator a few advantage. Since the large amplitude and high-frequency fields required to generate selection fields and to shift the positions of the magnetic fields are not used in this MPI system, it is free from health concerns that could be caused by high-energy alternating magnetic fields. It also has the advantage of being relatively safe and inexpensive to manufacture because it does not require a cooling system that is expensive to manufacture and maintain and uses small magnets.

We anticipate this approach to be applied to building MPI systems for diverse purposes, for example, not only to achieve high-resolution MPI at a smaller FOV but also to build medical MPI systems with larger FOVs, such as for human brain scanning, with an appropriate weight.

**Author Contributions:** T.K. contributed to the design and manufacture of the FFL generation system and wrote the main text. In addition, T.K. participated in the imaging acquisition experiment. J.C. contributed to the production of the equipment and software used in this paper. He also contributed to most of the experiments mentioned in the paper. B.S. assisted the experiments and reviewing the manuscript. H.H. contributed to the overall concept development, the experiments and reviewed the manuscript. H.-J.K. contributed to the concept development and reviewed the manuscript.

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**Institutional Review Board Statement:** In this section, you should add the Institutional Review Board Statement and approval number, if relevant to your study.

**Conflicts of Interest:** The authors declare no conflict of interest.

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